

A Peer Reviewed Open Access International Journal

## Permanent Deformation on Flexible Pavement; Rutting Effect on Bituminous Concrete Pavement



S.Subbarayudu Post Graduate Student Department of Civil Engineering, Lords Institute of Engineering & Technology, Himayath Nagar, Hyderabad.



Mohammed Abdul Hameed M.Tech(Phd) Professor & HoD Department of Civil Engineering, Lords Institute of Engineering & Technology, Himayath Nagar, Hyderabad.



Mohammed Haris M.Tech Associate Professor Department of Civil Engineering, Lords Institute of Engineering and Technology, Himayath Nagar, Hyderabad.

#### ABSTRACT

Pavements represent an important infrastructure to all countries. In India, huge investments have been made in constructing a large network. The network requires great care through conducting periodic evaluation and timely maintenance to keep the network operating under acceptable level of service. Pavement distress prediction and pavement condition prediction models can greatly enhance the capabilities of pavement management system. These models allow pavement authorities to predict the deterioration of the pavements and consequently determine needs and activities, predicting the timing of maintenance or rehabilitation, and estimating the long range funding requirements for preserving the performance of the network.

In this study, historical data of pavement distress forming five parameters of data is collected in low volume rural roads of three districts namely Guntur, Kurnool, and Warangal in the period of seven months. pavement condition ,pavement evaluation, predict parameters for the pavement and deterioration is the mathematical description that can be used to predict future pavement deterioration on present pavement condition based and deterioration factors .These data were categorized, processed, and analyzed.. These data have been

employed to generate prediction of pavement distress and condition models for the low volume rural roads of 15 stretches. Through the study, the most severely affected pavement distress type stretch is on HASANPARTHY TO NAGARAM (W13) having been identified. The behavior of these distress types has been investigated. A linear regression function was found to be an excellent representation of the data. Five for rural main pavement distress models have been developed. However, more comprehensive pavement condition models have also been developed, for rural main condition .the developed models provide a reasonable prediction of pavements condition. The models were assessed by standard error and residual analysis. By taking the soil tests, rut, raveling, cracking, pothole, edge failures are measured with the help of load man or vertical measurements steel rod to find outing the deformation of flexible pavement based on traffic data and substituting this all requires equations to find out Root Man Square error value. Comparing the RMS value to actual values obtain in the field in validation to conclude the percentage of error where is heavy by above comparisons due to this to knowing the serviceability of road.

Keywords: Low volume road, granular pavement, pavement evaluation, Pavement deterioration.



A Peer Reviewed Open Access International Journal

#### **INTRODUCTION**

India has more than 3.3 million kilometres of road network out of which Low Volume Roads (LVRs) accounts for 2.7 million kilometres which includes Other District Roads (ODRs) and Village Roads (VRs). LVRs are the tertiary road system in total road network which provides accessibility for the rural habitations to market and other facility centres. In India, during the last five decades, LVRs are being planned and programmed in the context of overall rural development, and tried to provide "all weather connectivity" with some level of achievement.

More than 80 percent of roadway mileage in the world carries less than 200 vehicles per day and would therefore be classified as LVRs (Gourley and Greening 1999). Traffic conditions in rural area are distinctly different from major roads. A variety of vehicles are used for transportation of goods on rural roads, ranging from animal drawn bullock-carts to the fast moving commercial vehicles. LVRs form a critical link to the nation for better transportation system, and to provide mobility to the rural areas. The development of rural infrastructure is crucial for the sustainable development of rural economic as well as the welfare of the poor people in rural areas. Inadequate rural connectivity and lack of mobility creates serious constraint to accelerated rural development. The critical role played by roads in economy development is being realized now.

#### **NEED FOR THE STUDY**

The application of pavement management techniques in India have been recognized recently as versatile tools for tackling road maintenance and rehabilitation problems. To establish these strategies, pavement performance data over a period of time is required for the development of appropriate deterioration models. Without adequate data, the road needs cannot be quantified or evaluated accurately, and planning decisions tend to become short-term. It is important, therefore, to identify which parameters are essential and relevant as predictive models. A number of studies have been conducted in general for high volume roads, but very few studies have been conducted on low volume roads. Most of the studies, such as the AASHTO, Kenyan and Brazilian studies were performed considering only the prevailing conditions of the respective regions.

Traffic conditions on low volume roads are distinctly different from other roads. Dawson et al. (2007) observed that many of the low volume roads are distressed due to over loaded local trucks, commercial vehicles, environmental factors such as temperature and precipitation etc. In addition to these factors, rutting, ravelling, roughness and cracking are also the main contributing factors of pavement failure. With this back ground, in the present study, an attempt has been made to identify the factors influencing performance of low volume roads. Pavement deterioration models have been developed for low volume roads considering three years in-service flexible pavement data. Following pavement deterioration models have been developed in this dissertation work: rutting model, cracking model, pothole model, ravelling model, and edge drop model.

#### **OBJECTIVES OF THE STUDY**

The main objectives of this study are listed below:

- 1. To review the concept of pavement deterioration and the factors associated with the performance for low volume roads.
- 2. To determine the rate of deterioration of low volume roads considering various material, traffic, and climatic conditions through systemic data collection.
- 3. To develop pavement deterioration models for various distress types prevailing in low volume roads.

# Criteria for Selection of Pavement Sections for Evaluation

The pavement sections in the present study have been selected based on the following criteria:

The selected test stretch should comprise of flexible pavement on a fairly ground, preferably on low embankment without a steep gradient.



A Peer Reviewed Open Access International Journal

- The length of test section selected is 500 m starting from a land mark in this case, sign board of PMGSY or kilometre stone of the road.
- The road condition should be uniformly good without any undulations, ruts and other distresses. There should not be any water logging conditions, culverts etc. within the test sections.
- Section is selected on straight reaches and not on curved portions. Also, approaches to bridge and culverts were avoided. History of the pavement section should be available i.e., year of construction, crust details and traffic volume counts, etc.

| S.No | Name of the test R<br>section       |     | District     | Subgrad<br>e Soil<br>type     | Rainfall<br>intensity<br>(mm/yr) | Traffic<br>volume<br>Curve | Surface<br>type |
|------|-------------------------------------|-----|--------------|-------------------------------|----------------------------------|----------------------------|-----------------|
| 1    | Chakaraypalem To<br>Davuluru        | G1  |              | B.C soil                      | >1000                            | В                          | BT              |
| 2    | Yeletipalem to<br>Dhulupudi         | G2  | Guntur       | B.C/silt<br>mixed             | >1000                            | С                          | BT              |
| 3    | Palem To Kollimerla                 | G3  | Guntur       | B.C soil                      | >1000                            | С                          | BT              |
| 4    | Loyapally To<br>Zendapetathanda     | G4  |              | Silty /<br>Mixed red<br>earth | 500-1000                         | С                          | BT              |
| 5    | Midthur To Kazipeta                 | К5  |              | B.C soil/<br>HG soil          | 500-1000                         | В                          | BT              |
| 6    | Aspari To Haligera                  | K6  | Kurnool      | B.C soil                      | 500-1000                         | A                          | BT              |
| 7    | Joannagiri To Pendekal              | K7  |              | Grave/BC                      | 500-1000                         | A                          | BT              |
| 8    | NH -18 To Gottlur                   | K8  | 1            | B.C soil                      | 500-1000                         | В                          | BT              |
| 9    | Tarigoppala To Abdul<br>Nagaram     | W9  |              | Gravel                        | 500-1000                         | В                          | вт              |
| 10   | Station Ghanpur To<br>Sreepathpally | W10 |              | Gravel                        | >1000                            | В                          | BT              |
| 11   | Veldhi To Ashwaraopally             | W11 | Mananaa      | Gravel                        | 500-1000                         | В                          | BT              |
| 12   | Edupusalapally to<br>Kommagudem     | W12 | Waranga<br>l | Gravel                        | >1000                            | В                          | BT              |
| 13   | Hasanparthy To<br>Nagaram           | W13 |              | B.C soil                      | 500-1000                         | В                          | BT              |
| 14   | Somidi To Subbayyapally             | W14 |              | B.C soil                      | 500-1000                         | С                          | BT              |
| 15   | PWD road To Singaram                | W15 |              | B.C soil                      | 500-1000                         | В                          | BT              |

#### DETAILED DESCRIPTION OF STUDY AREAS

#### FIELD AND LABORATORY STUDIES



Figure 1 shows atypical cracking pattern PWD Singaram Stretch

| Road<br>ID | Traffic (msa)    |             |                   |               |             |  |  |  |  |  |  |  |
|------------|------------------|-------------|-------------------|---------------|-------------|--|--|--|--|--|--|--|
|            | Januar<br>y 2015 | Feb<br>2015 | Marc<br>h<br>2015 | April<br>2015 | May<br>2015 |  |  |  |  |  |  |  |
| G1         | 0.02             | 0.030       | 0.06              | 0.08          | 0.23        |  |  |  |  |  |  |  |
| G2         | 0.014            | 0.024       | 0.033             | 0.05          | 0.105       |  |  |  |  |  |  |  |
| G3         | 0.078            | 0.090       | 0.111             | 0.153         | 0.28        |  |  |  |  |  |  |  |
| G4         | 0.009            | 0.009       | 0.017             | 0.026         | 0.101       |  |  |  |  |  |  |  |
| K5         | 0.029            | 0.033       | 0.045             | 0.079         | 0.111       |  |  |  |  |  |  |  |
| K6         | 0.01             | 0.019       | 0.026             | 0.094         | 0.359       |  |  |  |  |  |  |  |
| K7         | 0.041            | 0.043       | 0.045             | 0.079         | 0.111       |  |  |  |  |  |  |  |
| K8         | 0.01             | 0.020       | 0.02              | 0.07          | 0.11        |  |  |  |  |  |  |  |
| W9         | 0.045            | 0.047       | 0.081             | 0.093         | 0.126       |  |  |  |  |  |  |  |
| W10        | 0.012            | 0.048       | 0.05              | 0.111         | 0.16        |  |  |  |  |  |  |  |
| W11        | 0.038            | 0.048       | 0.062             | 0.101         | 0.112       |  |  |  |  |  |  |  |
| W12        | 0.072            | 0.072       | 0.081             | 0.125         | 0.245       |  |  |  |  |  |  |  |
| W13        | 0.046            | 0.057       | 0.08              | 0.103         | 0.118       |  |  |  |  |  |  |  |
| W14        | 0.056            | 0.062       | 0.071             | 0.084         | 0.111       |  |  |  |  |  |  |  |
| W15        | 0.059            | 0.072       | 0.109             | 0.836         | 0.925       |  |  |  |  |  |  |  |

Table 1 Traffic data during the study periods

| Road<br>ID | Characteristic Rut depth(mm) |             |                   |               |             |              |              |  |  |  |  |  |  |
|------------|------------------------------|-------------|-------------------|---------------|-------------|--------------|--------------|--|--|--|--|--|--|
|            | Januar<br>y<br>2015          | Feb<br>2015 | Marc<br>h<br>2015 | April<br>2015 | May<br>2015 | June<br>2015 | July<br>2015 |  |  |  |  |  |  |
| G1         | 4.9                          | 7.3         | 9.1               | 10.1          | 11.3        | 19.4         | 26.1         |  |  |  |  |  |  |
| G2         | 36.4                         | 43.4<br>5   | 45.3              | 46.7          | 47.3        | 48.8         | 52.3         |  |  |  |  |  |  |
| G3         | 3.9                          | 5.4         | 7.7               | 9.5           | 12.3        | 16.1         | 22.9         |  |  |  |  |  |  |
| G4         | 8.1                          | 12.6        | 13.8              | 16.3          | 20.1        | 26.4         | 36.8         |  |  |  |  |  |  |
| K5         | 14.7                         | 26.6        | 37.4              | 39.7          | 39.7        | 42.6         | 47.6         |  |  |  |  |  |  |
| K6         |                              |             | 16.7              | 18.5          | 18.5        | 20.1         | 31.8         |  |  |  |  |  |  |
| K7         | 13.4                         | 14.3        | 15.6              | 18.1          | 18.1        | 21.3         | 39.3         |  |  |  |  |  |  |
| K8         | 18.4                         | 24.4        | 26                | 27.4          | 27.4        | 28.9         | 37.5         |  |  |  |  |  |  |
| W9         | 2.64                         | 7.45        | 8.9               | 9.7           | 11.6        | 13           | 15.4         |  |  |  |  |  |  |
| W10        | 1.72                         | 5.83        | 5.6               | 7.5           | 10.5        | 12           | 15.4         |  |  |  |  |  |  |
| W11        | W11 1.88                     |             | 9.1               | 8.2           | 10.9        | 14.3         | 19           |  |  |  |  |  |  |
| W12        | 8.42                         | 9.13        | 12.4              | 13.9          | 17.4        | 24.4         | 26.3         |  |  |  |  |  |  |
| W13        | 5.8                          | 12.0<br>2   | 19.5              | 23.9          | 26.6        | 27.5         | 29.1         |  |  |  |  |  |  |
| W14        | 8                            | 11.9<br>8   | 22.5              | 24.4          | 29.9        | 35           | 49.8         |  |  |  |  |  |  |
| W15        | 10.3                         | 15.4<br>1   | 25                | 32.7          | 35.9        | 43.3         | 59.8         |  |  |  |  |  |  |

Table 2 Characteristic rut depth during study period



A Peer Reviewed Open Access International Journal

| Road code | Atterberg | sums<br>(%) |     |       |       | Grain S | Size Ana  | alysis |       |      | ition,             | Hea<br>Compa |       | re (%)             | BR   | pe ( |  |
|-----------|-----------|-------------|-----|-------|-------|---------|-----------|--------|-------|------|--------------------|--------------|-------|--------------------|--|------|--|
|           | Att       |             | PI  |       | %     | Passing | g IS Siev | /es(mn | ı)    |      | ifice              | MDD          | OMC   | istu               | Moisture<br>oaked CBF<br>.%<br>Unsoaked<br>CBR (%) |      |  |
|           | LL        | PL          | (%) | 4.75  | 2.0   | 0.6     | 0.425     | 0.212  | 0.075 | dust | IS Classification, | (gm/cc)      | (%)   | Field Moisture (%) | Soaked CBR<br>Value %                              | Unse |  |
| G1        | 30        | 16          | 14  | 76.54 | 62.44 | 31.22   | 22.56     | 9.47   | 0.40  | 0    | SP                 | 1.80         | 16.23 | 20                 | 3  | 24   |  |
| G2        | 46        | 23          | 23  | 50.67 | 42.28 | 19.79   | 15.44     | 6.45   | 0.15  | 0    | SP                 | 1.45         | 31.34 | 41                 | 3  | 24   |  |
| G3        | 27        | 13          | 14  | 64.95 | 39.53 | 15.31   | 10.98     | 4.28   | 0.23  | 0    | SP                 | 1.92         | 13.37 | 8                  | 6  | 28   |  |
| G4        | 48        | 25          | 23  | 75.55 | 55.59 | 35.79   | 32.58     | 20.72  | 0.49  | 0    | SP                 | 1.37         | 24.82 | 11.8               | 3  | 28   |  |
| K5        | 30        | 16          | 14  | 96.05 | 84.04 | 58.48   | 43.41     | 13.81  | 0.36  | 0    | SP                 | 1.91         | 14.57 | 10                 | 4  | 24   |  |
| K6        | 29        | 15          | 14  | 58.50 | 48.31 | 31.33   | 24.44     | 12.81  | 0.25  | 0    | SP                 | 1.68         | 14.70 | 18                 | 6  | 13   |  |
| K7        | 28        | 16          | 12  | 63.59 | 28.23 | 12.99   | 11.39     | 7.38   | 0.16  | 0    | SP                 | 1.94         | 11.85 | 9.3                | 5  | 24   |  |
| K8        | 46        | 25          | 21  | 67.39 | 52.74 | 25.36   | 17.15     | 6.89   | 0.13  | 0    | SP                 | 1.75         | 19.11 | 14                 | 10   | 18.  |  |
| W9        | 32        | 16          | 16  | 84.9  | 54.7  | 26.4    | 20.8      | 11.3   | 3.8   | 0    | SW                 | 1.65         | 13.33 | 12                 | 5  | 21   |  |
| W10       | 32        | 16          | 16  | 89.1  | 65.2  | 30.4    | 23.9      | 10.9   | 2.2   | 0    | SW                 | 1.62         | 13    | 14                 | 5  | 18   |  |
| W11       | 32.5      | 13.4        | 18  | 86.1  | 67.4  | 36.5    | 30.4      | 15.7   | 2.6   | 0    | SW                 | 1.71         | 15.25 | 10                 | 6  | 20   |  |
| W12       | 30        | 16          | 14  | 86.1  | 67.4  | 36.5    | 30.4      | 15.7   | 2.6   | 0    | SP                 | 1.68         | 14.21 | 13                 | 5  | 20   |  |

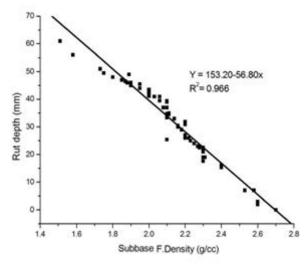


Figure 2 Variation of measured rut depth with

#### Sub-base field density for G1 stretch

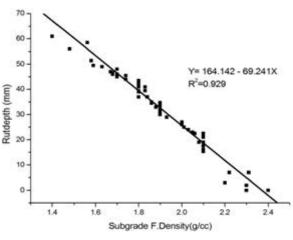


Figure 3 Variation of measured rut depth with

Volume No: 2 (2015), Issue No: 8 (August) www.ijmetmr.com

Sub grade field density for G1 stretch

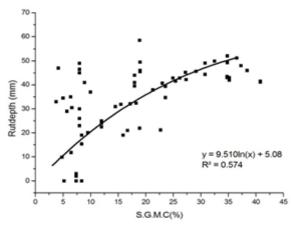


Figure 4 Variation of measured rut depth with

#### Sub-base moisture content for G1 stretch

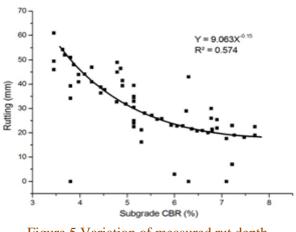


Figure 5 Variation of measured rut depth

#### with Sub-grade CBR for G1 stretch

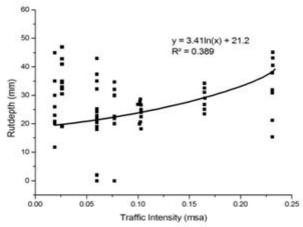


Figure 6 Variation of measured rut depth with Traffic intensity for G1 stretch



A Peer Reviewed Open Access International Journal

| Chainage       |       | Rut           | Field Den | sity(g/cc) | Subgrade<br>moisture | Subgrade | Traffic            |  |
|----------------|-------|---------------|-----------|------------|----------------------|----------|--------------------|--|
| From To        |       | depth<br>(mm) | Sub-base  | Subgrade   | content              | CBR (%)  | intensity<br>(msa) |  |
| 4/400          | 4/450 | 30.9          | 2.16      | 1.90       | (%)<br>14.5          | 4.20     | 0.231              |  |
| 4/450          | 4/500 | 0.0           | 2.70      | 2.30       | 8.4                  | 3.80     | 0.231              |  |
| 4/500          | 4/550 | 0.0           | 2.70      | 2.30       | 8.4                  | 3.80     | 0.231              |  |
| 4/550          | 4/600 | 15.4          | 2.35      | 2.13       | 8.4                  | 5.30     | 0.231              |  |
| 4/600          | 4/650 | 39.3          | 2.06      | 1.83       | 39.5                 | 3.80     | 0.231              |  |
| 4/650          | 4/700 | 33.4          | 2.13      | 1.87       | 34.1                 | 3.80     | 0.231              |  |
| 4/700          | 4/750 | 34.2          | 2.13      | 1.87       | 35.8                 | 3.80     | 0.231              |  |
| 4/750          | 4/800 | 16.2          | 2.35      | 2.13       | 22.7                 | 5.30     | 0.231              |  |
| 4/800          | 4/850 | 21.2          | 2.29      | 2.07       | 22.7                 | 5.30     | 0.231              |  |
| 4/850          | 4/900 | 31.9          | 2.16      | 1.90       | 15.5                 | 3.80     | 0.231              |  |
| 4/400          | 4/450 | 34.7          | 2.13      | 1.87       | 23.6                 | 6.87     | 0.077              |  |
| 4/450          | 4/500 | 0.0           | 2.70      | 2.30       | 5.2                  | 7.12     | 0.077              |  |
| 4/500          | 4/550 | 0.0           | 2.70      | 2.30       | 5.2                  | 7.12     | 0.077              |  |
| 4/550          | 4/600 | 17.6          | 2.33      | 2.10       | 18.9                 | 7.12     | 0.077              |  |
| 4/600          | 4/650 | 45.3          | 1.90      | 1.70       | 41.6                 | 4.86     | 0.077              |  |
| 4/650          | 4/700 | 39.4          | 2.05      | 1.82       | 23.6                 | 4.86     | 0.077              |  |
| 4/700          | 4/750 | 41.5          | 2.03      | 1.80       | 40.8                 | 4.86     | 0.077              |  |
| 4/750          | 4/800 | 21.9          | 2.29      | 2.07       | 18.9                 | 6.87     | 0.077              |  |
| 4/800          | 4/850 | 25.4          | 2.13      | 1.87       | 18.9                 | 6.87     | 0.077              |  |
| 4/850          | 4/900 | 41.1          | 2.03      | 1.80       | 40.8                 | 4.86     | 0.077              |  |
| 4/400          | 4/450 | 37.0          | 2.08      | 1.84       | 31.7                 | 6.32     | 0.060              |  |
| 4/450          | 4/500 | 0.0           | 2.69      | 2.42       | 7.4                  | 6.32     | 0.060              |  |
| 4/500          | 4/550 | 0.0           | 2.69      | 2.42       | 7.4                  | 6 2 2    | 0.060              |  |
| 4/500          | 4/550 |               | -         |            |                      | 6.32     |                    |  |
| 4/550          | 4/600 | 19.0          | 2.31      | 2.08       | 15.9                 | 7.65     | 0.060              |  |
| 4/600          | 4/650 | 46.0          | 1.90      | 1.70       | 38.4                 | 6.32     | 0.060              |  |
| 4/650          | 4/700 | 42.0          | 2.00      | 1.78       | 35.2                 | 6.32     | 0.060              |  |
| 4/700          | 4/750 | 43.0          | 2.00      | 1.78       | 35.2                 | 6.32     | 0.060              |  |
| 4/750          | 4/800 | 22.5          | 2.29      | 2.07       | 27.4                 | 7.65     | 0.060              |  |
| 4/800          | 4/850 | 26.0          | 2.22      | 2.00       | 27.4                 | 7.65     | 0.060              |  |
| 4/850          | 4/900 | 43.0          | 2.00      | 1.78       | 35.2                 | 6.32     | 0.060              |  |
| 4/400          | 4/450 | 39.0          | 2.07      | 1.83       | 29.4                 | 5.97     | 0.060              |  |
| 4/450          | 4/500 | 2.0           | 2.64      | 2.28       | 7.4                  | 5.97     | 0.060              |  |
| 4/500          | 4/550 | 3.0           | 2.62      | 2.24       | 7.4                  | 5.97     | 0.060              |  |
| 4/550          | 4/600 | 21.0          | 2.30      | 2.07       | 16.7                 | 6.78     | 0.060              |  |
| 4/600          | 4/650 | 48.0          | 1.83      | 1.65       | 37.3                 | 5.97     | 0.060              |  |
| 4/650          | 4/700 | 43.0          | 1.97      | 1.76       | 34.8                 | 5.97     | 0.060              |  |
| 4/700          | 4/750 | 43.5          | 1.96      | 1.82       | 34.8                 | 5.97     | 0.060              |  |
| 4/750          | 4/800 | 21.5          | 2.29      | 2.09       | 26.9                 | 6.78     | 0.060              |  |
| 4/800          | 4/850 | 27.0          | 2.21      | 1.98       | 26.9                 | 6.78     | 0.060              |  |
| 4/850          | 4/900 | 46.0          | 1.87      | 1.68       | 34.9                 | 5.97     | 0.060              |  |
| 4/400          | 4/450 | 37.0          | 2.08      | 1.84       | 10.0                 | 6.78     | 0.019              |  |
| 4/450          | 4/500 | 7.0           | 2.53      | 2.22       | 8.3                  | 7.22     | 0.019              |  |
| 4/500          | 4/550 | 7.0           | 2.58      | 2.31       | 8.0                  | 7.22     | 0.019              |  |
| 4/550          | 4/600 | 23.0          | 2.27      | 2.05       | 8.0                  | 7.22     | 0.019              |  |
| 4/600          | 4/650 | 49.0          | 1.89      | 1.63       | 8.0                  | 4.79     | 0.019              |  |
| 4/650          | 4/700 | 45.0          | 1.89      | 1.70       | 8.0                  | 4.79     | 0.019              |  |
| 4/700          | 4/750 | 45.0          | 1.90      | 1.70       | 8.0                  | 4.79     | 0.019              |  |
| 4/750          | 4/800 | 26.0          | 2.22      | 2.00       | 8.0                  | 6.78     | 0.019              |  |
| 4/750<br>4/800 |       | 30.0          | 2.22      | 1.90       | 8.0                  | 6.78     | 0.019              |  |
|                | 4/850 | 46.5          | 1.87      | 1.90       | 8.0                  | 4.86     | 0.019              |  |
| 4/850          | 4/900 |               |           |            |                      |          |                    |  |
| 4/400          | 4/450 | 34.5          | 2.11      | 1.86       | 5.0                  | 5.14     | 0.026              |  |
| 4/450          | 4/500 | 56.0          | 1.58      | 1.48       | 10.6                 | 3.80     | 0.026              |  |
| 4/500          | 4/550 | 29.0          | 2.18      | 1.93       | 5.7                  | 6.25     | 0.026              |  |
| 4/550          | 4/600 | 41.0          | 2.03      | 1.80       | 8.9                  | 4.25     | 0.026              |  |
| 4/600          | 4/650 | 30.5          | 2.16      | 1.90       | 6.6                  | 5.14     | 0.026              |  |
| 4/650          | 4/700 | 35.0          | 2.11      | 1.86       | 6.4                  | 5.14     | 0.026              |  |
| 4/700          | 4/750 | 33.0          | 2.14      | 1.88       | 3.8                  | 5.14     | 0.026              |  |
| 4/750          | 4/800 | 47.0          | 1.85      | 1.67       | 4.2                  | 4.25     | 0.026              |  |
| 4/800          | 4/850 | 19.0          | 2.31      | 2.08       | 8.4                  | 4.25     | 0.026              |  |
| 4/850          | 4/900 | 51.0          | 1.73      | 1.58       | 9.8                  | 3.80     | 0.026              |  |
| 4/400          | 4/450 | 22.5          | 2.28      | 2.06       | 12.0                 | 5.14     | 0.103              |  |
| 4/450          | 4/500 | 25.0          | 2.23      | 2.01       | 12.0                 | 5.14     | 0.103              |  |
| 4/500          | 4/550 | 61.0          | 1.51      | 1.40       | 26.0                 | 3.45     | 0.103              |  |
| 4/550          | 4/600 | 44.0          | 1.95      | 1.74       | 18.0                 | 3.97     | 0.103              |  |
| 4/600          | 4/650 | 49.5          | 1.75      | 1.59       | 19.0                 | 3.45     | 0.103              |  |
| 4/650          | 4/700 | 39.5          | 2.06      | 1.83       | 18.0                 | 5.14     | 0.103              |  |
|                |       | 34.0          | 2.25      | 2.02       |                      | F 14     | 0.102              |  |
| 4/700          | 4/750 | 24.0          | 2.25      | 2.03       | 12.0                 | 5.14     | 0.103              |  |
| 4/750          | 4/800 | 46.0          | 1.88      | 1.68       | 19.0                 | 3.45     | 0.103              |  |
| 4/730          |       |               |           |            |                      |          |                    |  |
| 4/750<br>4/800 | 4/850 | 41.0          | 2.06      | 1.83       | 18.0                 | 3.97     | 0.103              |  |

Table 4 Summary of rut depth and different factors considered for G1 stretch

the model development using influencing For parameters, different forms of equations were tried and the form represented by Equation(1) has been selected. Similar models were developed for individual stretches. For explanatory purpose the following equation of G1 stretch is presented here.

## RD<sub>G1</sub> = -32.758 \* (SBFD) - 19.485 \* (SGFD) + 3.597 \* Ln (SGMC) - 0.035 \* (CBR) 2590 + 2.396

\* Ln (N) + 25.489

(1)

R<sup>2</sup>= 0.982, F-test =76.22 and Standard error = 2.16

Where,

SBFD = sub-base field density,

SGFD = subgrade field density,

SGMC = subgrade moisture content,

CBR = subgrade CBR (%), and

N = traffic intensity (msa).

The general form of the rutting model for individual stretches and combined district models with coefficients a, b, c, d etc., are represented by Equations (2) and (3). The complete analysis with the corresponding statistical significance is shown in Table 5.2.

(2)RD = a \* (SBFD) + b \* (SGFD) + c \* Ln (SGMC) + d \* (CBR) + f \* Ln (N) + g

RD = a \* (SBFD) + b \* (SGFD) + c \* Ln (SGMC) + d \* (CBR)° + f \* Ln(N) + g \* (Base G.III) + h \* (Base G.II)<sup>i</sup> + j \* (Sub BG)<sup>k</sup> + 1 (3)



A Peer Reviewed Open Access International Journal

| Coeffici<br>ents   | Road ID     |        |             |            |        |             |            |            |            |        |            |            |             |             |   |
|--------------------|-------------|--------|-------------|------------|--------|-------------|------------|------------|------------|--------|------------|------------|-------------|-------------|---|
|                    | G1          | G2     | G3          | G4         | GM     | K5          | K6         | K7         | K8         | KM     | W9         | W10        | W11         | W12         |   |
| a                  | -<br>32.758 | 42.099 | -5.51       | •0.25      | -4.58  | 13.129      | ·1.724     | 0.308      | •8.467     | 11.606 | 2.891      | -3.438     | -<br>12.063 | 19.555      | - |
| b                  | 19.485      | ·1.513 | -5.577      | •5.537     | 30.424 | 10.264      | -0.078     | 0.045      | -0.649     | -0.902 | 13.22      | -4.873     | -9.387      | -5.186      |   |
| c                  | 3.597       | 1.233  | 13.993      | 7.873      | 7.763  | 2.963       | 0.446      | 0.218      | 6.532      | 0.078  | 8.962      | 6.802      | 5.769       | 4.17        |   |
| d                  | -0.035      | -9.914 | -<br>40.816 | ·11.88     | -0.016 | -<br>19.797 | -0.348     | -<br>0.776 | -0.361     | 18.742 | -<br>4.059 | -0.328     | -2.396      | -<br>38.567 |   |
| e                  | 2.59        | -0.358 | -0.209      | -0.655     | 2.627  | -0.41       | 0.387      | 0.345      | 1.872      | -0.474 | 0.113      | 1.118      | 11.291      | -4.278      |   |
| f                  | 2.396       | 0.561  | 3.592       | 1.232      | 0.656  | 1.158       | 0.04       | 0.226      | 0.652      | 1.201  | 1.642      | 0.626      | 0.445       | 2.522       |   |
| g                  | 25.489      | 21.723 | 23.041      | 12.20<br>8 | 20.145 | 29.164      | -1.133     | 0.678      | 40.16<br>5 | 21.308 | 17.62      | 14.64<br>1 | -0.464      | 93.502      |   |
| h                  |             |        |             |            | 0.606  |             |            |            |            | 0.063  |            |            |             |             |   |
| i                  |             |        |             |            | -8.543 |             |            |            |            | -0.591 |            |            |             |             |   |
| j                  |             |        |             |            | 1.27   |             |            |            |            | 0.127  |            |            |             |             |   |
| k                  |             |        |             |            | 16.373 |             |            |            |            | -3.662 |            |            |             |             |   |
| 1                  |             |        |             |            | 0.321  |             |            |            |            | 0.32   |            |            |             |             |   |
| R-<br>square       | 0.982       | 0.979  | 0.797       | 0.765      | 0.777  | 0.891       | 0.794      | 0.73       | 0.799      | 0.821  | 0.756      | 0.757      | 0.852       | 0.729       |   |
| F-test             | 76.23       | 83.56  | 87.97       | 25.47      | 73.18  | 184.52      | 276.4<br>7 | 46.86      | 19.49      | 145.72 | 57.89      | 29.39      | 61.21       | 195.55      |   |
| Standar<br>d error | 2.16        | 0.79   | 4.31        | 4.25       | 8.08   | 3.44        | 1.39       | 4.11       | 4.43       | 4.53   | 1.69       | 2.62       | 3.34        | 1.33        |   |

Table 5 Coefficients of Rutting Models for all the stretches

#### VALIDATION OF THE MODEL

The validation of the model is done by utilizing the field data obtained from the selected test section and the predicted values from the developed models. Figure 5.62 shows the relation between observed rut depth and the predicted rut depth.

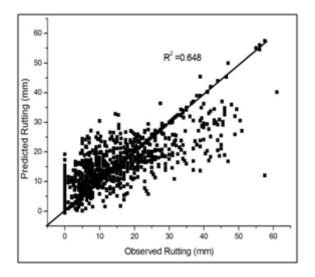


Figure 7 Relation between the observed and predicted rut depth

As the  $R^2$  value is more than 0.6, this indicates a good relation between the observed and predicted rut depth values. Figure 5.63 shows the relation between observed cracking and the predicted cracking. As the  $R^2$  value is more than 0.6, this indicates a good relation between the observed and predicted cracking values.

#### CONCLUSIONS

Based on the field studies and analysis the following conclusions are

- The influence of field density of the sub-base and field density of the subgrade materials on the observed rut depth is much higher when compared to other independent variables considered in this study. It was observed in most of the cases of all the selected stretches that with the increase field density, there is a decrease in the rut depth. The coefficient of determination is also found to be significantly high. The decrease in rut depth with increase in field density is due to the fact that the resistance of a material to permanent deformation will increase with increase in the density thus resulting in lower rut depths.
- The subgrade moisture content showed good correlation with rut depth in all the fifteen stretches of the roads considered in this study i.e. with the increase in subgrade moisture content, there is an increase in the rut depth. Because of increase in the moisture content, the subgrade gets weaker and one can expect an increase in the rut depth.
- Among all the parameters considered for the development of rutting model, base course (WBM grading III) gradation is found to have least influence on the rut depth.
- The influence of pavement age, camber and longitudinal gradient on the observed Pothole is much higher when compared to other independent variables considered in this study where as traffic intensity has lower influence on Pothole.
- By considering all the fifteen stretches of specified variables the ultimate model was developed for Pothole. The coefficient of



A Peer Reviewed Open Access International Journal

determination  $(\mathbb{R}^2)$  value is 0.792. It is important to note that the CBR, Traffic Intensity, Mean Monthly Precipitation, No. of Potholes, Pavement Age, Stripping Value, Camber and Longitudinal Gradient could not explain 20% of the observed cracking values.

- ▶ Stripping Value of aggregate and traffic are found to greatly affect the raveling whereas pavement age has least contribution to raveling. For the raveling model the coefficient of R<sup>2</sup> value is 0.894. It is important to note that the Pavement Age, Mean Monthly Precipitation, Stripping Value, Traffic intensity, Camber and Longitudinal Gradient could not explain 10% of the observed.
- The influence of camber, longitudinal gradient and traffic on the observed Edge failure is much higher when compared to other independent variables considered in this study where as pavement age has lower influence on Edge failure.
- The coefficient of determination (R<sup>2</sup>) value is 0.828. It is important to note that the Camber, Longitudinal Gradient, Traffic intensity, CBR and Modulus of elasticity of the shoulder material could not explain 17% of the observed edge failure values.
- During the study period among all the 15 stretches it has been observed that Hasanparthy to Nagaram (W13) stretch is severely affected by the factors considered whereas the least affected stretch is found to be Tarrigopula to Abdul Nagaram (W9).

#### **SCOPE FOR FURTHER WORK**

One can extend the same work using this data to develop deterioration models by all these parameters for few more years. To evaluate the performance of the pavements with proper maintenance, continuous study for successive years is required. For that this study is to be continued and historical data has to be generated. In addition to this test track with all the control conditions in the laboratory can also be incorporated in future study.

#### REFERENCES

Darter, M. (1980). "Requirement for Reliable Predictive Pavement Models." *Transportation Research Board*, No. 766, Washington, D.C.

- AASHTO. (1980). "Construction Manual For Highway Construction." Developed by the Highway Subcommittee on Construction, American Association of State Highway and Transportation Officials, Washington, DC.
- Montgomery, D. and Peck, E. (1982). "Introduction to Linear Regression Analysis." John Wiley & Sons, USA.
- Gilchrist, W. (1984). "Statistical Modelling." John Wiley & Sons, UK.
- Butler, B., Carmichael, R., and Flanagan, P. (1985). "Impact of Pavement Maintenance on Damage Rate", Federal Highway Administration (FHWA) Report.
- Peterson, D.E. (1987). "Pavement Management Practice." NCHRP synthesis No. 135, *Transportation Research Board*, National Research Council, pp. 12-41.
- Lytton, R. (1987). "Concept of pavement performance prediction and modeling." North American Conference on Managing Pavement, Toronto, Canada, No. 234.
- Organization for Economic Co-Operation and Development (OECD) (1987), "Pavement management systems", A report prepared by the OECD scientific expert group, OECD, Paris.



A Peer Reviewed Open Access International Journal

- Hosmer, D., and Lemeshow, S. (1989). "Applied Logistic Regression", John Wiley & Sons, USA.
- Lee, Y., Mohseni, A., and Darter, M. (1993). "Simplified Pavement Performance Models." *Transportation Research Record*, TRR 1344, Washington, D.C.
- Fekpe, E., and Okine, N. O. A. (1995). "Deterioration Modelling for lateritic-base flexible pavements." *Construction and Building Materials*, Vol.9 No.3, pp.159-163.