

Design & Analytical Investigation of the Performance of Dual Pressure Condenser in a Thermal Power Plant

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Abstract

In this thesis, analytical investigations are done to determine the efficiency of the dual pressure condenser in a thermal power plant for two fluids water and R600a. 3D model of the condenser is done in Creo. CFD and thermal analysis are done on the condenser by applying parameters calculated for high pressure condenser and low pressure condenser calculated theoretically. Thermal analysis is done to determine heat transfer rates by varying materials of the condenser. Analysis is done in Ansys.

1. DUAL PRESSURE CONDENSER

Large power plant condensers are usually 'shell and tube' heat exchangers where the two fluids do not come in direct contact and the heat released by the condensation of steam is transferred through the walls of the tubes into the cooling water continuously circulating inside them. In a "Dual pressure condenser" the two shells operate at different pressures. The bottom sides (hot well) of both the condensers are connected. For the convenience of cleaning and maintenance, cooling water flows through the tubes and steam condenses outside the tubes. These condensers can be classified based on the cooling water flow as single or multi pressure, depending on whether the cooling water flow path creates one or more turbine back pressures and thereby increasing the turbine efficiency. Dual pressure condensing system is incorporated with two condensers. These condensers have different internal pressure from each other and are installed below the each low pressure turbines LPT-A & LPT-B.

2. LITERATURE SURVEY

This paper is intended to review the literature on research, development and projects related to gas turbine combined cycle. It focuses on summarizing several research investigations carried out by the author and associates, during the past years, in the field of gas turbine combined system. The performance of gas-steam combined cycle power plant depends on various operating parameters. [4] In this study, the analysis has been applied to the typical 210MW (LMZ) plant in India. Designed of thermal power plant is based on conditions (like a good quality of steam, pressure and temperature of steam etc.), but actual outlet conditions are not as per the designed values. In practical, when power plants are installed there are lots of constraints. It has been observed that the design specified condenser vacuum is not maintained in most of the Indian thermal power stations, consequences of which invariably remain the poor efficiency, more costly generation and financial burden to the consumers. This paper deals with the factors or parameters which reduced the efficiency of the condenser.

3. THEORETICAL CALCULATIONS

Performance of low pressure condenser Cooling waterside 'Q' is calculated from the relationship:

$$Q_{Gain} = mC \times Cp (Tw2 - Tw1) \text{ ----- (A)}$$

Where

Tw1 is the inlet cooling water temperature (0C)

Tw2 is the outlet cooling water temperature (0C)

mC is the cooling water flow rate (kg/sec)

C_p is the specific heat of water, which may be assumed to be 4.19 kJ/kg 0C

Calculation of LMTD for series flow configuration

LMTD of LOW pressure condenser (ΔT_m) - B:

T_{w1} is the inlet cooling water temperature (oC)

T_{w2} is the outlet cooling water temperature (oC)

Let us assume that the inlet temperature of steam & the outlet temperature of condensate below the condenser are same (since the latent heat alone is removed in condenser).

$$T_m \text{ (LP condenser-B)} = \frac{(T_c - T_{w1}) - (T_c - T_{w2})}{\ln \frac{(T_c - T_{w1})}{(T_c - T_{w2})}}$$

LMTD of HIGH pressure condenser (ΔT_m)-A

T_{w2} is the inlet cooling water temperature (0C)

T_{w3} is the outlet cooling water temperature (0C)

Let us assume that the inlet temperature of steam & the outlet temperature of condensate below the condenser are same (since the latent heat alone is removed at condenser).

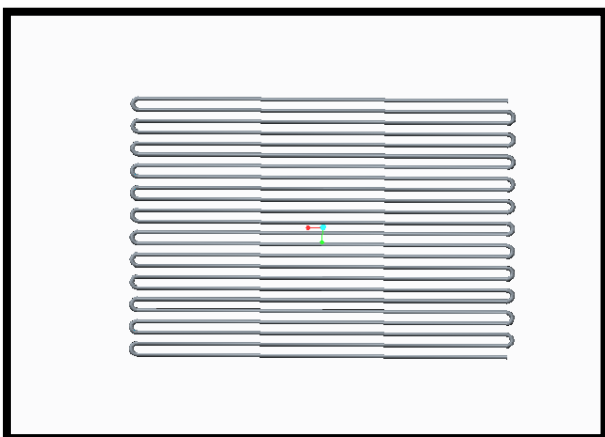
Effectiveness of condenser in series flow

$$\text{(For design value)} = \frac{(T_{w2} - T_{w1})}{T_s - T_{w1}}$$

4. MODELING OF DUAL PRESSURE CONDENSER

The model is designed from based on journal of plate-fin-and-tube condenser performance and design for refrigerant R-410A air-conditioner.

A. 3D Model of Condenser

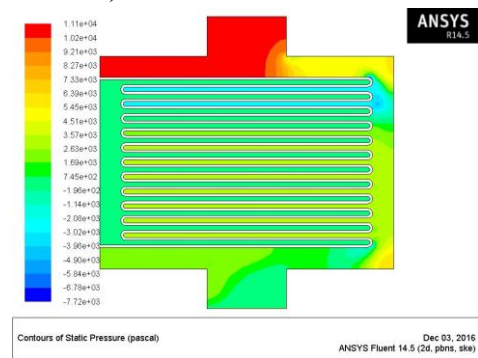


5. CFD ANALYSIS AND THERMAL ANALYSIS OF HIGH PRESSURE AND LOW PRESSURE CONDENSER

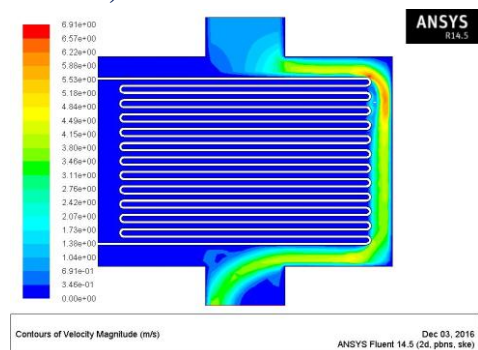
Analysis is done based on journal of ISSN 0976 – 6340 (Print) ISSN 0976 – 6359 (Online)

A. CFD ANALYSIS OF FLUID –R600a FOR HIGH PRESSURE CONDENSER

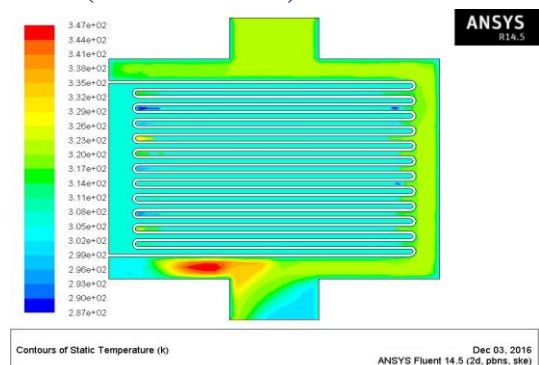
(i) PRESSURE RESULTS FOR CFD ANALYSIS (FLUID –R600a)



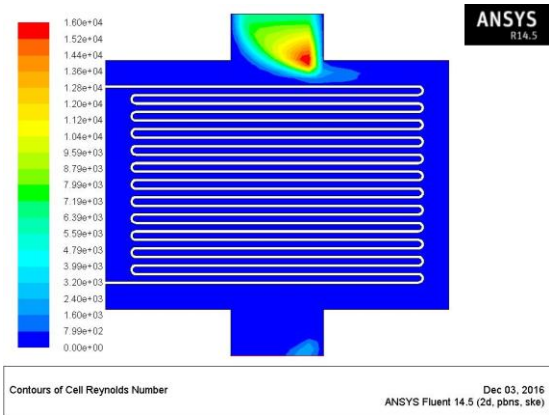
(ii) VELOCITY RESULTS FOR CFD ANALYSIS (FLUID –R600a)



(iii) TEMPERATURE RESULTS FOR CFD ANALYSIS (FLUID –R600a)



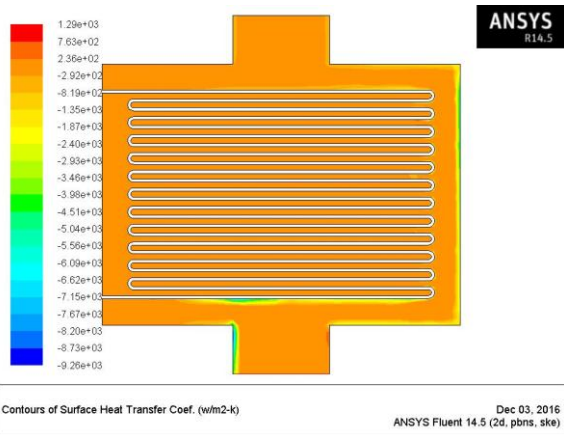
(iv) REYNOLD NUMBER RESULTS FOR CFD ANALYSIS (FLUID –R600a)



Total Heat Transfer Rate (w)

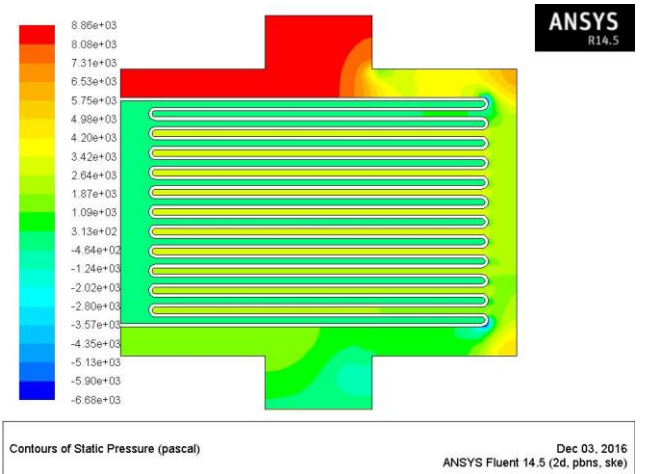
steam_inlet	8072870.5
steam_outlet	-7803734.5
wall_trm_srf	-110746.66
water_wall_surface	-115334.73
Net	43054.617

(v) SURFACE HEAT TRANSFER CO-EFFICIENT RESULTS FOR CFD ANALYSIS (FLUID – R600a)

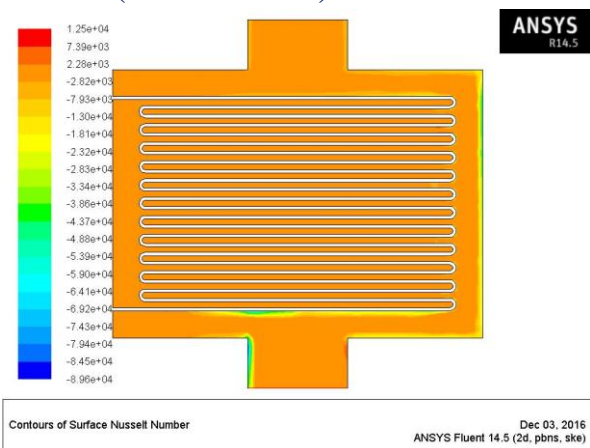


B. CFD ANALYSIS OF FLUID –R600a FOR LOW PRESSURE CONDENSER

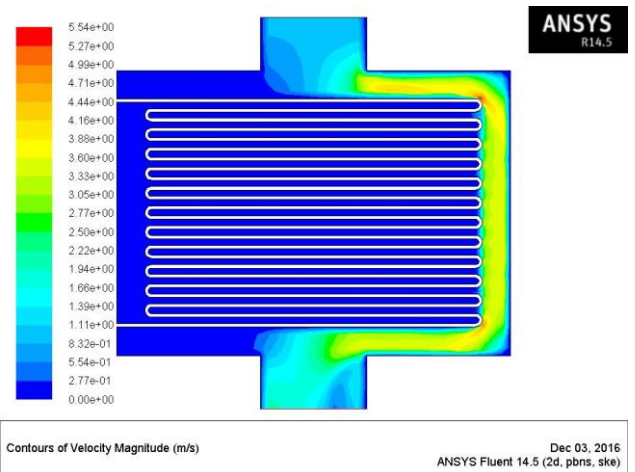
(i) PRESSURE RESULTS FOR CFD ANALYSIS (FLUID –R600a)



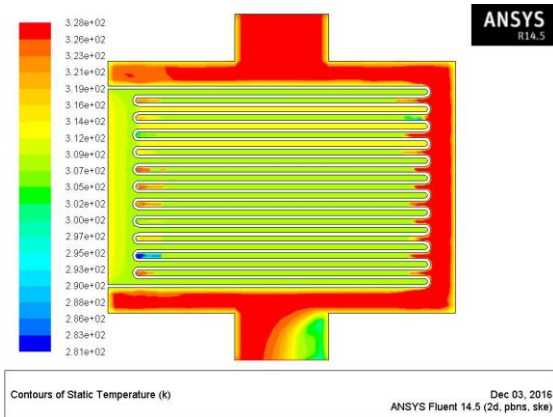
(vi) Nusselt NUMBER RESULTS FOR CFD ANALYSIS (FLUID –R600a)



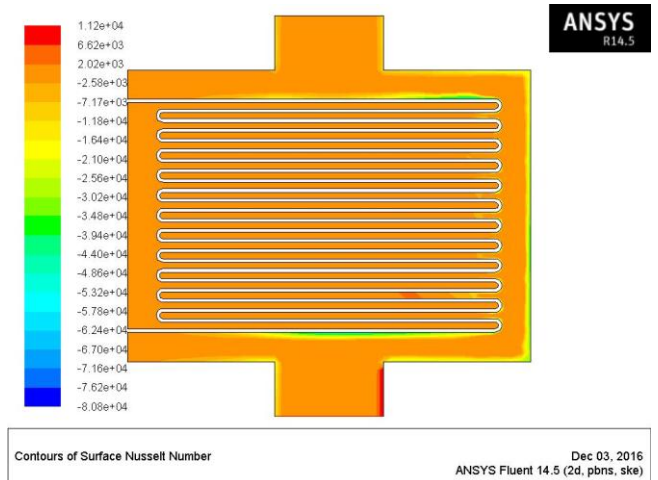
(ii) VELOCITY RESULTS FOR CFD ANALYSIS (FLUID –R600a)



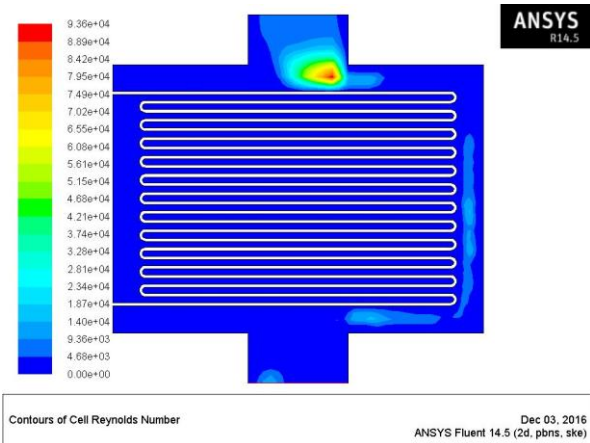
(iii) TEMPERATURE RESULTS FOR CFD ANALYSIS (FLUID –R600a)



(vi) Nusselt NUMBER RESULTS FOR CFD ANALYSIS (FLUID –R600a)



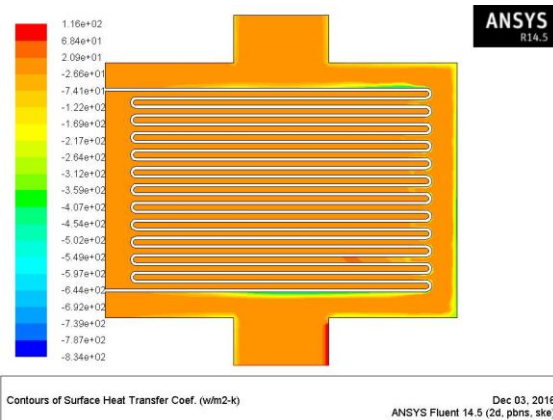
(iv) REYNOLD NUMBER RESULTS FOR CFD ANALYSIS (FLUID –R600a)



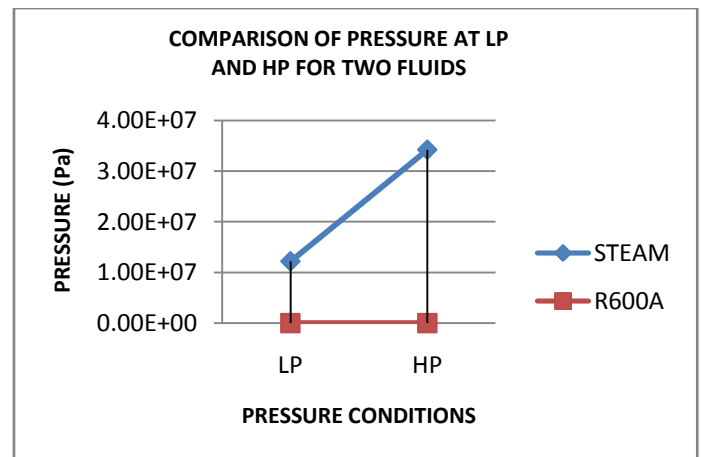
Total Heat Transfer Rate (w)

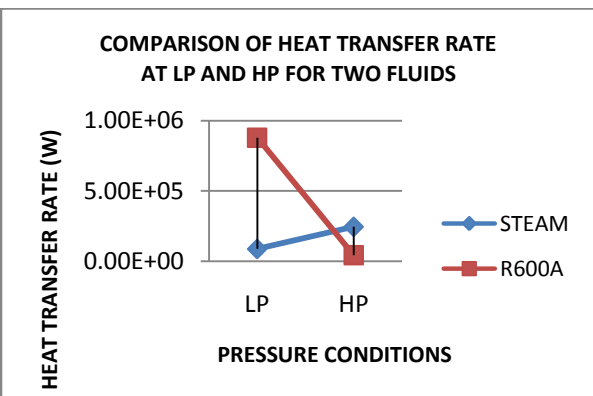
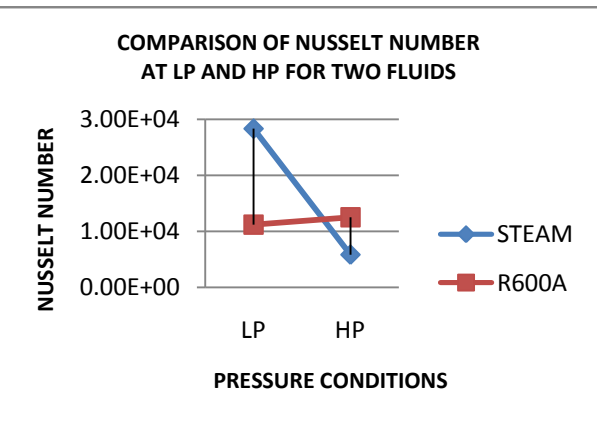
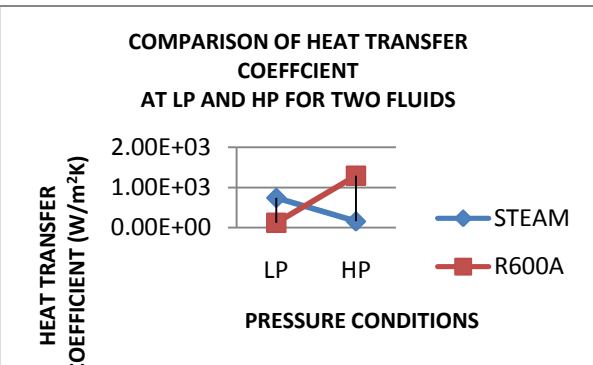
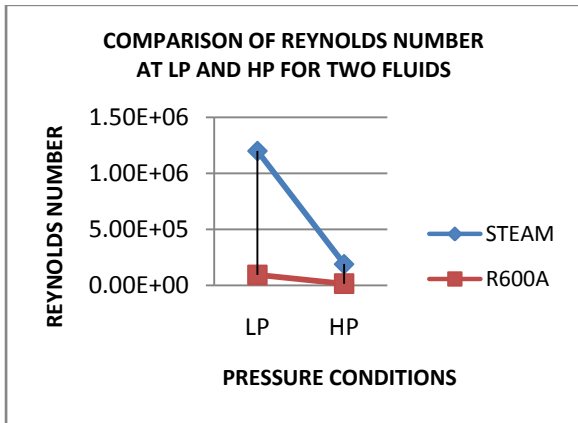
steam_inlet	10369299
steam_outlet	-11213735
wall_trm_srf	-13229.405
water_wall_surface	-19743.186
Net	-877408.59

(v) SURFACE HEAT TRANSFER CO-EFFICIENT RESULTS FOR CFD ANALYSIS (FLUID – R600a)



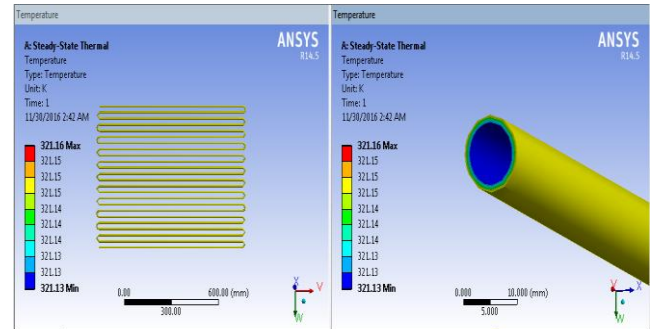
GRAPH COMPARISONS FOR TWO DIFFERENT FLUIDS FOR BOTH HIGH PERESSURE AND LOW PRESSURE CONDENSER



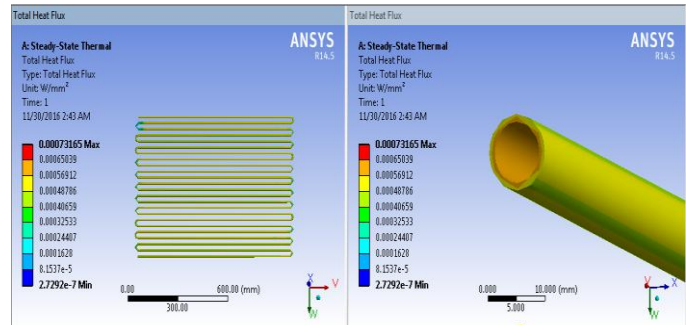


C.THERMAL ANALYSIS FOR DUAL PRESSURE CONDENSER

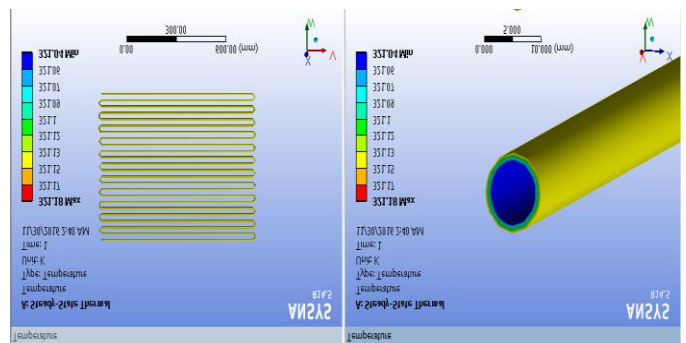
(i) TEMPERATURE RESULTS FOR THERMAL ANALYSIS (FLUID –R600a) HIGH PRESSURE CONDENSER MATERIAL – ALUMINUM



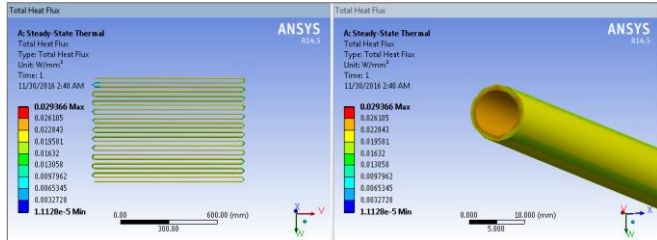
(ii) HEAT FLUX RESULTS FOR THERMAL ANALYSIS (FLUID –R600a) HIGH PRESSURE CONDENSER MATERIAL – ALUMINUM



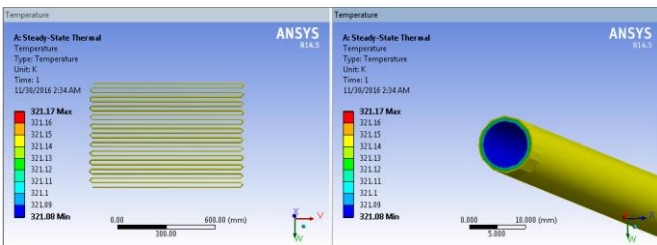
(iii) TEMPERATURE RESULTS FOR THERMAL ANALYSIS (FLUID –R600a) HIGH PRESSURE CONDENSER MATERIAL – BRASS



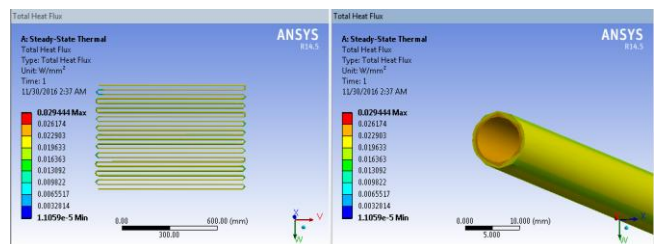
(iv) HEAT FLUX RESULTS FOR THERMAL ANALYSIS (FLUID –R600a) HIGH PRESSURE CONDENSER MATERIAL – BRASS



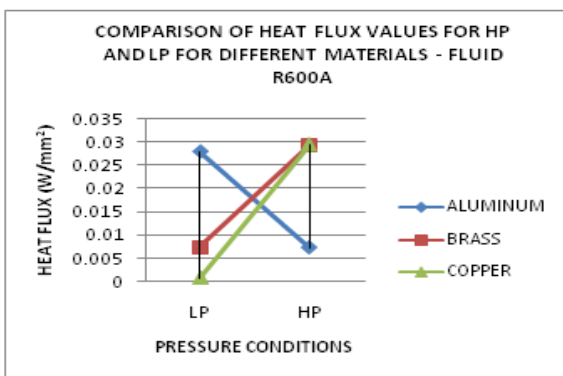
(v) TEMPERATURE RESULTS FOR THERMAL ANALYSIS (FLUID –R600a) HIGH PRESSURE CONDENSER MATERIAL – COPPER



(vi) HEAT FLUX RESULTS FOR THERMAL ANALYSIS (FLUID –R600a) HIGH PRESSURE CONDENSER MATERIAL –COPPER



GRAPH COMPARISONS FOR THREE DIFFERENT MATERIALS AT LOW PRESSURE AND HIGH PRESSURE.



6.CONCLUSION

The thermal efficiency of a power plant can be increased by enhancing the heat transfer rate of a condenser; this can be achieved by reducing the temperature and pressure of the condensate while leaving the condenser. From the CFD analysis results, the pressure is reduced from high pressure condenser to the low pressure condenser, the velocity is increasing from high pressure condenser to low pressure condenser. The temperature is reduced from high pressure condenser to the low pressure condenser. The heat transfer rate is also increasing. By observing thermal analysis results, the heat flux is increasing in Low pressure condenser. That is the heat transfer rate is increasing when the condensate is leaving the condenser.

7. ACKNOWLEDGMENT

I would like to express my profound gratitude and deep regards to Mr.K. RAJASEKHARA REDDY for his exemplary guidance, monitoring and constant encouragement throughout the course of this thesis. The blessing, help and guidance given by beloved principal shall carry them a long way in the journey of life on which they are about to embark.

8.REFERENCES

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