

## Enhance the Power Flow in the Power System Network by Using UPFC Mechanism

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### ABSTRACT

*In a power systems, power flows from the generating centre's to the load centres. In this process many things require investigation, such as the profile of the bus voltage, flow of active power (MW) and reactive power (MVar) in transmission lines, effect of rearranging circuits and installation of regulating devices etc., for different loading conditions. As modern power system has become more large and complex, these investigations should be done with some sort of simulation of the system. Hence in order to meet power demand in a very efficient and economical way, by incorporating Unified Power Flow Controller Device (UPFC) in the transmission system and by using Congestion Management which is used in this project and it makes possible to handle practically all power flow control and transmission line compensation problems, using Solid State Controllers, which provide functional flexibility. The Unified Power Flow Controller (UPFC) is a member of Flexible AC transmission system (FACTS) device, that utilizes the synchronous voltage sources (VSC) to provide comprehensive control of traditional power flow concepts, the UPFC able to control simultaneously or selectively, all the parameters such as voltage, Impedance, phase angle that affect the power flow in a transmission line. In other words it can provide functional capabilities of controlling both the active and reactive power independently. This project aims to present a reliable method to meet the requirements by developing an N-R based load flow calculation program through which control settings of the UPFC*

*can be determined directly. The proposed method keeps the N-R load flow algorithm intact and requires only a little modification to the Jacobian matrix in the iterative procedure. A Mat lab program has been developed to calculate the control settings parameters of the UPFC after the load flow is converged. The proposed method is tested on standard IEEE-14 bus system.*

**Keywords:** UPFC; FACTS (TCSC, TCRP); Optimal Power Flow Algorithm (N-R Method); Mat Lab;

### INTRODUCTION

As the power systems are becoming more complex it requires careful design of the new devices for the operation of controlling the power flow in transmission system, which should be flexible enough to adapt to any momentary system conditions. The operation of an ac power transmission line, is generally constrained by limitations of one or more network parameters and operating variables. By using FACTS technology [1] such as STATCON (Static Condenser), Thyristor Controlled Series Capacitor (TCSC), Thyristor controlled Phase angle Regulator (TCPR), UPFC etc., [2] the bus voltages, line impedances, and phase angles in the power system can be regulated rapidly and flexibly. FACTS do not indicate a particular controller but a host of controllers which the system planner can

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choose based on cost benefit analysis. The UPFC is an advanced power system device capable of providing simultaneous control of voltage magnitude and active and reactive power flows in an adaptive fashion. Owing to its instantaneous speed of response and unrivalled functionality, it is well placed to solve most issues relating to power flow control in modern power systems. The UPFC can control voltage, line impedance and phase angles in the power system[1] which will enhance the power transfer capability and also decrease generation cost (and improve the security and stability) of the power system. UPFC can be used for power flow control, loop flow control, load sharing among parallel corridors in this paper UPFC is treated to operate in closed loop form and control parameters of UPFC are derived to meet the required power flow along the line.

## UPFC MODEL FOR POWER FLOW STUDIES

### Principles of UPFC:

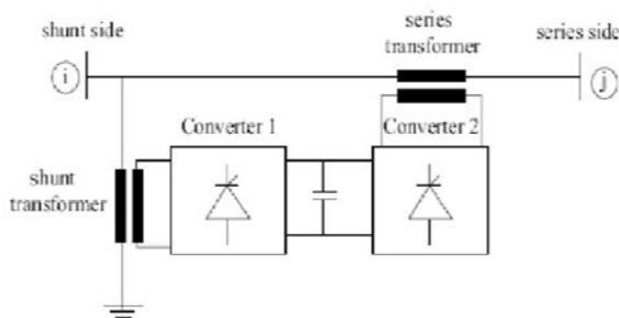


Figure 1: Implementation of the UPFC by Back-To-Back Voltage Source Converters

The UPFC can provide simultaneous control of transmission voltage, impedance and phase angle of transmission line. It consists of two switching converters as shown in figure 1.

These converters are operated from a common D.C link provided by a D.C storage capacitor. Converter 2 provides the power flow control of UPFC by injecting an ac voltage with controllable magnitude and phase angle in series with the transmission line via a series transformer [3]. Converter one is to absorb or supply the real power demand by the converter 2 at the common

D.C link. It can also absorb or generate controllable reactive power and provide shunt reactive power compensation. The UPFC concept provides a powerful tool for cost effective utilization of individual transmission lines by facilitating the independent control of both the real and reactive power flow and thus the maximization of real power transfer at minimum losses in the line.

### Power Injection Model of UPFC:

The two voltage source model of UPFC is converted in to two power injections in polar form for power flow studies with approximate impedances as shown in figure2.

The advantage of power injection representation is does not destroy the symmetric characteristics of admittance matrix. When formulated in polar form, the power flow equations are quadratic. Some numerical advantages can be obtained from the form. The polar form also leads naturally to the idea of an optimal power flow; this will be discussed in next section. The voltage sources can be represented by the relation- ship between the voltages and amplitude modulation ratios and phase shift of UPFC [4]. In this model the shunt transformer impedance and the transmission line impedance including the series transformer impedance are assumed to be constant. No power loss is considered with the UPFC.

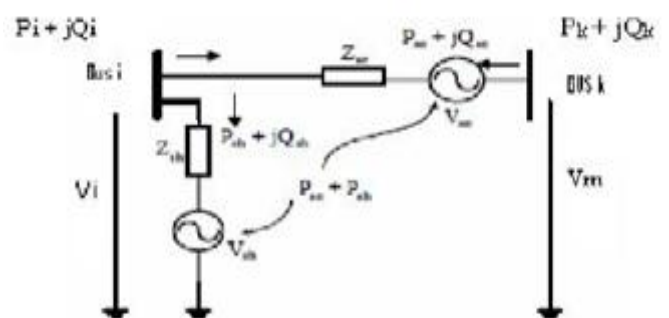


Figure 2: Two Voltage Source Model of UPFC

### Steady State UPFC Representation:

There are two aspects in handling the UPFC in steady state analysis:

1. When the UPFC parameters are given, a power flow program is used to evaluate the impact of the given UPFC on the system under various conditions. In this case UPFC is operated in open loop form. The corresponding power flow is treated as normal power flow.

2. As UPFC can be used to control the line flow and bus voltage, control techniques are needed to derive the UPFC control parameters to achieve the required objective. In this case UPFC is operated in closed loop form. The corresponding power flow is called controlled power flow.

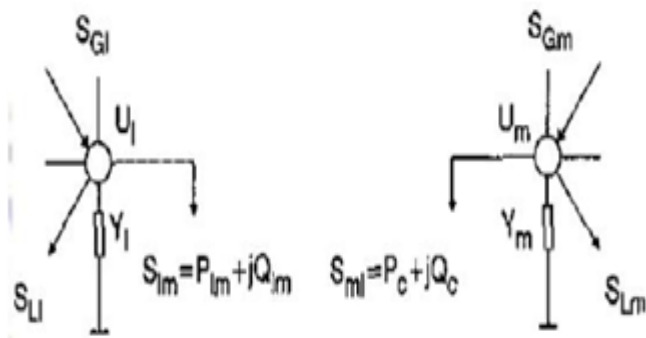


Figure 3: Steady State Model of UPFC Connected Between Bus 1 and M

For a given control strategy, the power Sm1 on the UPFC-controlled transmission line l-m is set to constant (Pc + jQc). By means of the substitution theorem, this branch l-m can be detached as shown in Figure.3. In which Sm1, represents power from the bus m and Sm1, from the bus 1. For each other additional UPFC, its corresponding branch can be dealt with similarly [5].

**PROBLEM FORMULATION OF UPFC FOR POWER FLOW STUDIES**

**Load Flow Problem**

In this paper the load flow problems are solved by using N-R method in polar co-ordinate form is an iterative method which approximates the set of linear simultaneous equations using Taylor's series expansion and the terms are limited to first Approximation. In the power flow of the transmission line the complex power injected at the ith bus with respect to ground system is

$$S_i = P_i + jQ_i = V_i I_i^*$$

Where  $i=1,2,3,\dots,n$

Where  $V_i$  is the voltage at the  $i^{th}$  bus with respect to ground and  $I_i$  is the source current injected is the bus.

$$P_i + jQ_i = V_i I_i^*$$

$$I_i = \sum_{k=1}^n Y_{ik} V_k$$

Equating real and imaginary parts

$$P_i = \text{Real} [V_i^* \sum_{k=1}^n Y_{ik} V_k]$$

$$Q_i = -\text{imag} [V_i^* \sum_{k=1}^n Y_{ik} V_k]$$

$$V_i = |V_i| e^{j\delta_i}$$

$$Y_{ik} = |Y_{ik}| e^{j\theta_{ik}}$$

Real power reactive power now be expressed as

$$P_i \text{ (Real power)} = |V_i| \sum_{k=1}^n |V_k| |Y_{ik}| \cos(\theta_{ik} + \delta_k - \delta_i)$$

$$Q_i \text{ (Reactive power)} = |V_i| \sum_{k=1}^n |V_k| |Y_{ik}| \sin(\theta_{ik} + \delta_k - \delta_i);$$

$i=1, 2, 3, 4, \dots, n; i \neq \text{slack bus}$

**UPFC Modified Jacobian Matrix Elements:**

In power flow the two power injections ( $P_i, Q_i$ ) and ( $P_j, Q_j$ ) of a UPFC can be treated as generators however because they vary with the connected bus bar voltage amplitudes and phases the relevant elements of Jacobin matrix at each iteration. The formation of Jacobian matrix [6].

$$\begin{bmatrix} \Delta P \\ \Delta Q \end{bmatrix} = \begin{bmatrix} H & N \\ J & L \end{bmatrix} \begin{bmatrix} \Delta \delta \\ |\Delta V| \end{bmatrix}$$

Where H, N, J, L are the elements of jacobian matrix,

$$H_{im} = \frac{\partial P_i}{\partial \delta_m};$$

$$N_{im} = \frac{\partial P_i}{\partial |V_m|};$$

$$L_{im} = \frac{\partial Q_i}{\partial |V_m|};$$

$$J_{im} = \frac{\partial Q_i}{\partial \delta_m};$$

The elements of Jacobin matrix calculated as follows

Case 1:  
 $m \neq i$   
 $H_{im} = L_{im} = a_m f_i - b_m e_i$   
 $N_{im} = -J_{im} = a_m e_i - b_m f_i$   
 Where  
 $Y_{im} = G_{im} + jB_{im}$   
 $V_i = e_i - jf_i$   
 $(a_m + jb_m) = (G_{im} + jB_{im}) * (e_i - jf_i)$

Case 2:  
 $m = i$   
 $H_{ii} = -Q_i - B_{ii}|V_i|^2$   
 $N_{ii} = P_i + G_{ii}|V_i|^2$   
 $J_{ii} = P_i - G_{ii}|V_i|^2$   
 $L_{ii} = Q_i - B_{ii}|V_i|^2$

### Optimum Power Flow Algorithm:

In this paper optimal power flow algorithm is adopted as it offers a number of advantages that is to detect the distance between the desired operating point and the closest unfeasible point. Thus it provides a measure of degree of controllability and it can provide computational efficiency without destroying the advantages of the conventional power flow when used error feedback adjustment to implement UPFC model [8]. The proposed model and algorithm as follows:

1. Form the Admittance Matrix from the given line data
2. By using N-R method calculates the jacobian elements
3. Modify the jacobian matrix (after placing UPFC in the system)
4. Modify the mismatch power equation
5. Update system Bus bars Voltages
6. Check for convergence otherwise repeat the same process
7. Print the Load flow information, bulbar voltages, generations, Line flows, and Transmission losses.

### UPFC IMPLEMENTATION IN POWER FLOW STUDIES

The Implementation of UPFC models in power flow is essentially a controlled power flow problem. The UPFC modelling needs the change of relevant elements of Jacobin matrix however the user defined power flow

software do not allow users to directly modify the Jacobian matrix and only provide the facilities for the iteration between the main program and user defined model. This iteration sometimes diverges especially when the system is heavily loaded.

### Control Strategies of UPFC

In this section the UPFC represented by two voltage sources of series path and shunt path is often transformed in to a pair of power injections ( $P_i, Q_i$ ), ( $P_j, Q_j$ ) at both sides of UPFC Locations in order to be incorporated into power flow algorithm. From the view point of effects of these power injections on the system  $Q_i$  can be independently regulated to support bus bar voltage connected at the shunt path  $P_i$  and  $P_j$  are used to manipulate line active power with equal magnitude but at reverse direction and  $Q_j$  can control both  $j$  bus bar voltage and line reactive power based on this analysis the philosophy of the UPFC local control strategy is described [9]. After modifying all the UPFC connected branches, the load flow equations can be written as follows:

$$P_i + jQ_i = V_i^* \sum_{k=1}^n Y_{ik} V_k \quad i \neq l, m$$

$$P_l + jQ_l = V_l^* \sum_{k=1}^n Y_{lk} V_k + (P_{lm} + jQ_{lm})$$

$$P_m + jQ_m = V_m^* \sum_{k=1}^n Y_{mk} V_k + (P_c + jQ_c)$$

With the above modifications the load flow studies should be done, after convergence the control settings of UPFC can be determined as follows. 1. Use  $Q_i$  to control bus voltage  $V_i$  2. Use  $P_i$  and  $P_j$  to control the line power. 3. Set  $Q_j = 0$  (i.e. better to use  $Q_i$  to control  $V_i$  since it is closer to the bus). 4. The feedback information of power injections ( $P_i, Q_i$ ) ( $P_j, Q_j$ ) derived from the above closed loop controllers is then converted into UPFC control parameters [10].

### CASE STUDY AND CONCLUSION

#### Case Study:

In order to investigate the feasibility of the proposed technique, a large number of power systems of different sizes and under different system conditions have been tested. It should be pointed out that the results are under

so-called normal power flow, i.e. the control parameters of UPFC are given and UPFC is operated in a closed-loop form. All the results indicate good convergence and high accuracy achieved by the proposed method. In this section, the IEEE 14-bus practical system [11] has been presented to numerically demonstrate its performance. It has been used to show quantitatively, how the UPFC performs. The original network is modified to include the UPFC. This compensates the line between any of the buses.

The UPFC is used to regulate the active and reactive power flowing in the line at a pre specified value. The load flow solution for the modified network is obtained by the proposed power flow algorithm and the Mat lab program is used to find the control setting of UPFC for the pre specified real and reactive power flow between any buses and the power flow between the lines are observed the effects of UPFC [12, 13]. The same procedure is repeated to observe the power flow between the buses(Depending on the pre specified value of the active and reactive power the UPFC control setting is determined after the load flow is converged).

### Test Results for IEEE 14 Bus System:

The performance of UPFC on the IEEE 14 bus system shown in figure4.

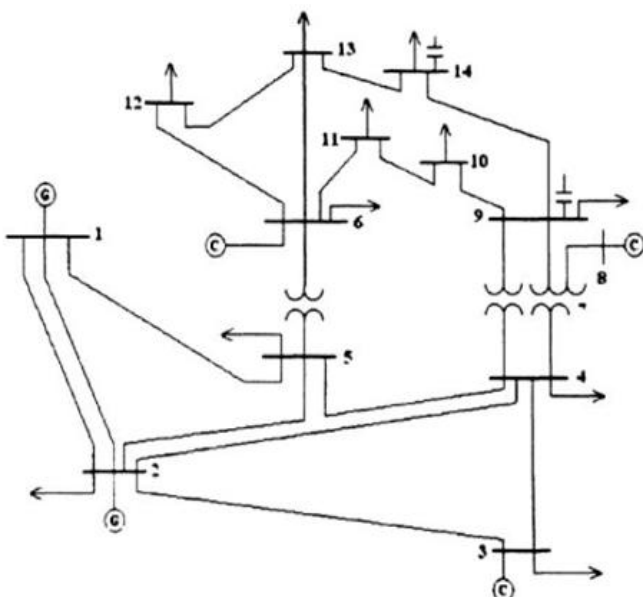


Fig 4: IEEE 14 bus system

### Test Results without UPFC:

The voltage profile of the system is tabulated below:

Bus	Voltage	Angle(rad)	Angle(deg)
1	1.060000	0.000000	0.000000
2	0.179331	-2.288247	-131.10686
3	3.003445	2.569834	147.240670
4	0.801914	1.153725	66.103578
5	0.557927	2.134085	122.274079
6	0.361504	0.632530	36.241286
7	1.205262	0.493703	28.287102
8	0.029187	0.237284	13.595389
9	0.200750	-1.509105	-86.465347
10	0.088059	1.616350	92.610029
11	0.095862	-1.698440	-97.313422
12	0.398357	1.836755	105.238306
13	1.116873	-0.412811	-23.652326
14	0.632956	2.982683	170.895172

The Power flow profile of the system

Bus code	Real power(Mv)	Reactive power(Mvar)	Loss
1-2	8.427942	18.311464	7.027357
1-5	-0.640964	6.581140	2.119981
2-3	2.496023	-0.825690	10.097645
2-4	0.503510	0.794991	1.601668
2-5	0.601350	0.152012	0.681603
3-4	29.240393	39.059395	17.718054
4-5	-5.324704	11.044104	3.120731
4-7	2.833800	-0.576041	0.0000
4-9	0.133342	1.413121	-0.000000
5-6	0.798388	1.179781	0.000000
6-11	0.404998	0.583696	0.366826
6-12	-0.306318	0.456276	0.284050
6-13	1.908977	-1.520838	3.015375
7-8	0.050649	8.053528	0.000000
7-9	1.997330	14.125655	0.000000
9-10	0.223268	0.602056	0.325453
9-14	0.472542	0.029734	0.707077
10-11	0.023820	0.073490	0.063149
12-13	1.870098	0.124471	4.890334
13-14	2.607364	4.269854	3.429823

**Test results with UPFC:**

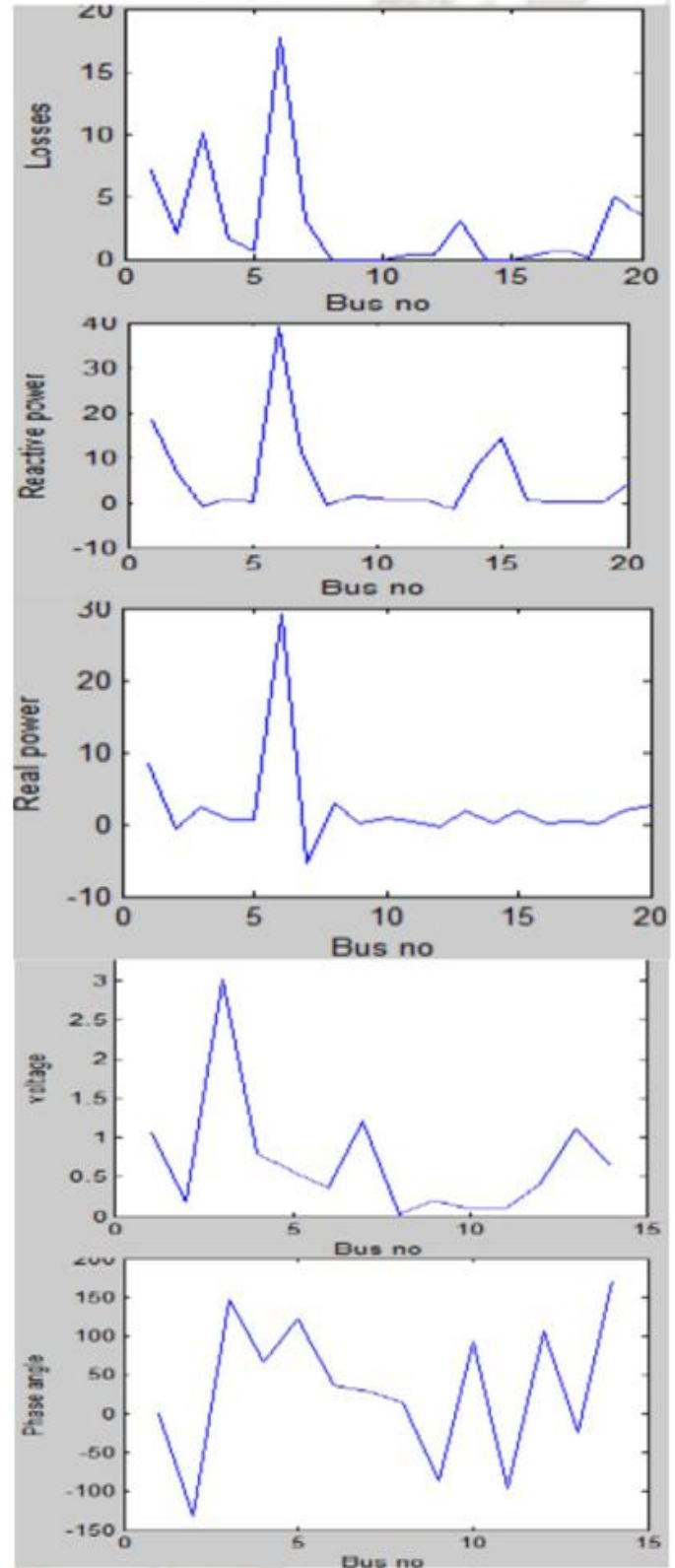
The voltage profile of the system is tabulated below:

Bus	Voltage	Angle(rad)	Angle(deg)
1	1.060000	0.000000	0.000000
2	1.137716	0.085501	4.898831
3	1.197531	0.187757	10.757695
4	1.185627	0.165721	9.495116
5	1.167506	0.142518	8.165699
6	1.206837	0.219664	12.585838
7	1.208420	0.206742	11.845449
8	1.208420	0.206742	11.845449
9	1.221203	0.227689	13.045600
10	1.225012	0.229993	13.177616
11	1.218993	0.226622	12.984494
12	1.219505	0.230963	13.233204
13	1.223628	0.231860	13.284619
14	1.237072	0.242100	13.871284

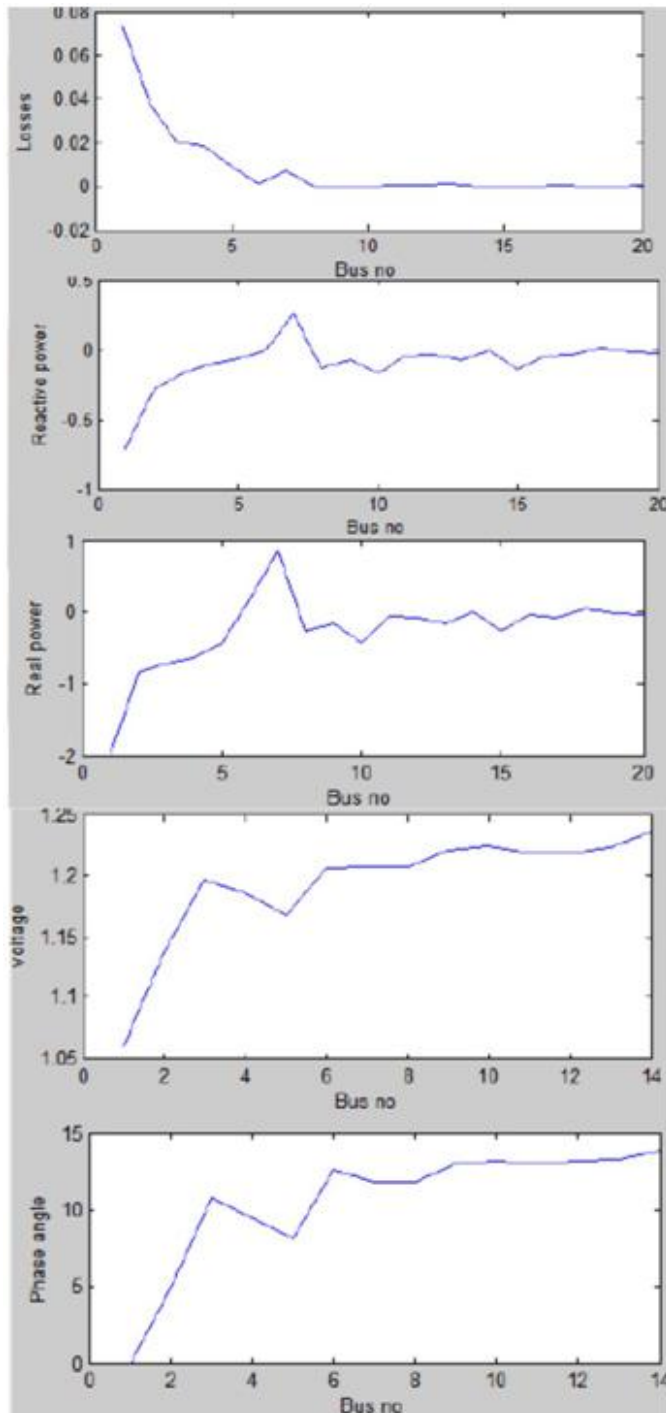
The Power flow profile of the system:

Bus code	Real power	Reactive power	loss
1-2	-1.961689	-0.704930	0.074240
1-5	-0.848453	-0.276779	0.037601
2-3	-0.734209	-0.161881	0.020217
2-4	-0.637580	-0.096423	0.018498
2-5	-0.447139	-0.058455	0.008854
3-4	0.187574	0.002699	0.001651
4-5	0.842512	0.251929	0.007344
4-7	-0.280967	-0.123464	0.000000
4-9	-0.161216	-0.070842	0.000000
5-6	-0.430879	-0.165576	-0.000000
6-11	-0.070517	-0.039904	0.000428
6-12	-0.075997	-0.022882	0.000532
6-13	-0.172365	-0.067185	0.001554
7-8	0.000000	0.000000	0.000000
7-9	-0.280967	-0.137476	0.000000
9-10	-0.053867	-0.034732	0.000088
9-14	-0.093316	0.027226	-0.000805
10-11	0.036046	0.023035	0.000100
12-13	-0.015529	0.007988	-0.000045
13-14	-0.054493	-0.020275	0.000386

**Graphs for without Incorporation of UPFC**



Graphs for with Incorporation of UPFC



CONCLUSION

The unified power flow controller provides simultaneous or individual controls of basic system parameters like Transmission voltage, impedance and phase angle, thereby controlling transmitted power. In this thesis an

IEEE 14 bus system is taken into consideration to observe the effects of UPFC. Load flow studies were conducted on given system to find the nodal voltages, and power flow between the nodes. The MATLAB program is run with and without incorporation of UPFC. UPFC is incorporated between any of two buses, to improve the power flow between the lines to a Pre-specified value. From the results it has been observed that the power flow between the lines is improved to a pre-specified value. The real power losses between the lines were decreased after the incorporation of UPFC. So, it can be concluded that after the incorporation of UPFC the voltage profile and power flow between the lines improves. Also by using this program, control setting of UPFC for different pre-specified power flows can be obtained.

REFERENCES

[1] Y. Morioka, Y. Mishima, and Y. Nakachi, "Implementation of unified power flow controller and verification of transmission capability improvement," IEEE Trans. Power Syst, vol. 14, pp. 575– 581, May 1999.

[2] P. C. Stefanov and A. M. Stankovic, "Modeling of UPFC operation under unbalanced conditions with dynamic phasors," IEEE Trans. Power Syst., vol. 17, pp. 395–1403, May 2002.

[3] H. F. Wang, "A unified model for the analysis of facts devices in damping power system oscillations part I: Single machine infinite-bus power systems," IEEE Trans. Power Delivery, vol. 12, pp. 941–946, Apr. 1997.

[4] "A unified model for the analysis of facts devices in damping power system oscillations part II: Multi-machine power systems," IEEE Trans. Power Delivery, vol. 13, pp. 1355–1361, Oct. 1998.

[5] "A unified model for the analysis of facts devices in damping power system oscillations part III: Unified power flow controller," IEEE Trans. Power Delivery, vol. 15, pp. 978– 983, July 2000.

[6] R. Mihilac, P. Zunko, and D. Povh, "Improvement of transient stability using unified power flow controller," IEEE Trans. Power Delivery, vol. 11, pp. 485–492, Jan. 1996

[7] K. R. PadiyarS and A. M. Kulkarni, "Control design and simulations of unified power flow controller," IEEE Trans. Power Delivery, vol. 13, pp. 1348–1354, Oct. 1998.

[8] I. Papic, P. Zunko, and D. Povh, "Basic control of unified power flow controller," IEEE Trans. Power Syst., vol. 12, pp. 1734–1739, Nov. 1997.

[9] C. Schauder, "Vector analysis and control of advanced static var compensators," in Proc. Inst. Elect. Eng. C, vol. 140, 1993, pp. 299–306.

[10] S. Kannan, S. Jayaram, and M. M. A. Salama, "Design of a de- coupled controller for a shunt converter: Control design and performance," in Proc. 32nd North American Power Symp., Waterloo, ON, Canada, Oct. 2000, pp. 8–13.

[11] P. K. Steimer, H. E. Gruning, E. Carroll, S. Klaka, and S. Linder, "IGCT: A new emerging technology for high power, low cost converters," in Proc. IEEE Industrial Applications Society, Annual Meeting, New Orleans, LA, Oct. 1997.

[12] W. L.Feng, H. W. Nagan: "control settings of Unified power flow controllers through a robust load flow calculations", IEEE proceedings on generation, transmission and distribution. Vol146. No. 4, July 1999.

[13] Nabavi-Naiki. A and iravani. M. R: "steady state and dynamic models of Unified power flow controller for power system studies", IEEE Transactions power systems, vol. 11, no. 4, nov 1996.