

Experimental Investigation on Pervious Concrete

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ABSTRACT:

Pervious concrete is a special type of concrete with a high porosity used for concrete flatwork applications that allows water from precipitation and other sources to pass directly through, thereby reducing the runoff from a site and allowing groundwater recharge. The high porosity is attained by a highly interconnected void content. Typically pervious concrete has little or no fine aggregate and has just enough cementations paste to coat the coarse aggregate particles while preserving the interconnectivity of the voids.

It is an important application for sustainable construction and is one of many low impact development techniques used by builders to protect water quality. Cost efficiency was the main motive due to a decreased amount of cement. Pervious concrete is a mixture of cement, coarse aggregate and water with little to no fine aggregates. The addition of a small amount of sand will increase the strength. Water to cement ratio of 0.27 to 0.40 with a void content of 15 to 25%.

Pervious concrete can attain a compressive strength ranging from 400 psi to 4000 psi (2.8 to 28 Mpa) though strengths of 600 psi to 1500 psi (2.8 to 10 Mpa) are more common. Pervious concrete can done in field as well as in laboratory. In Laboratory testing has shown that entrained air may improve the freeze thaw durability even when the pervious concrete is in a fully saturated condition. Pervious concrete mixture proportion is used for improving freeze thawing durability also.

1.INTRODUCTION:

Interest and use of Portland cement pervious concrete (PCPC) pavements is increasing in climates subject to severe winter environmental conditions. Because much of the experience with these pavements has been in warmer climates, some questions have been raised as to the durability of the material under freeze-thaw attack.

Although some laboratory tests suggest that PCPC is not freeze-thaw durable when saturated, proper design can insure the concrete is not saturated under field conditions. The best predictor of future field performance is actual past field performance.

In Northeast Ohio, interest in pervious concrete has been increasing. Extensive flooding in this region during the summer of 2006 will no doubt increase the level of interest substantially. Several demonstration projects have been completed.

1.1.Goals and Objectives:

The main objective of this study was to document the performance of pervious concrete pavements in freeze-thaw environments, in order to provide guidance as to how to construct durable PCPC pavements in these climates.

The secondary objective was to evaluate clogging of these pavements, and to estimate the effectiveness of maintenance procedures for restoring Infiltration capability to clogged installations where no preventive maintenance program was enacted.

1.2.Significance of the Project:

This project will help facilitate broader use of pervious concrete for pavements throughout North-America. This technology has been widely used across the south eastern U.S., particularly in Georgia and Florida.

As the use expands into regions where pavements are susceptible to freezing and thawing, questions of durability must be addressed. Other field Performance issues, such as clogging, are of interest in all regions.

2.MIX DESIGN OF PERVIOUS CONCRETE MIX:

Material	Mix1	Mix2	Mix3	Mix4
Cement (kg/m ³)	355.98	359.54	355.98	365.47
Coarse Aggregate, #89 (lb/yd ³)	1547.33	1560.37	1547.33	1587.07
Water (lb/yd ³)	96.11	96.71	96.14	11.45
w/cm	0.27	0.27	0.27	0.28

Table 1: Arterial properties

2.1 ADMIXTURES USED FOR THE CONCRETE MIX:

Admixtures	MIX1	MIX2	MIX3	MIX4
MRWR (ml/100 kg)	326.0	326.0	326.0	326.0
HCA (ml/100 kg)	326.0	326.0	326.0	326.0
VMA (ml/100 kg)	0	130.4	326.0	652.0

Table 2: Admixtures used

2.2 COMPRESSIVE STRENGTH TEST FOR CYLINDERS:

Compression test is the most common test conducted on hardened concrete, partly because it is an easy test to perform, and partly because most of the desirable characteristic properties of concrete are qualitatively related to its compressive strength. Compression test is carried out on specimens cubical in shape. Sometimes, the compression strength of concrete is determined using parts of beam tested in flexure.



**Fig.1:A cylindrical specimen is placing in the compression testing machine
The cylindrical specimen is of the size 15mm*300mm.**

2.3 SPLITTING TENSILE TEST FOR CYLINDER (15mm*300mm):

It is very difficult to measure the tensile strength of concrete directly. Of late some methods have been used with the help of epoxy bonded end pieces to facilitate direct pulling. Attempts have also been made to find out direct tensile strength of concrete by making briquette of figure 8 shape for direct pulling but this method was presenting some difficulty with grip and introduction of secondary stresses while being pulled.

Whatever may be the methods adopted for finding out the ultimate direct tensile strength, it is almost impossible to apply truly axial load. There is always some eccentricity present. The stress is changed due to eccentricity of loading. These may introduce major error on the stresses developed regardless of specimen size and shape.



Fig.2: A cylindrical specimen placing in horizontal direction in the machine

The 3rd problem is the stresses induced due to the grips. There is a tendency for the specimen to break near the ends. This problem is always overcome by reducing the section of the central portion of the specimen. The method in which sisal plates are glued with the epoxies to the ends of the test specimen, eliminate stresses due to gripping, but offers no solution for the development of eccentricity. SPLIT TENSILE TEST is sometimes also referred as BRAZILIAN TEST. This test was developed in Brazil. It is also known as indirect tension test method. The test carried out on the cylinder having 15cm diameter having 30cm height and by placing the cylindrical specimen horizontally between the loading surfaces of a compression testing machine and the load is applied until the failure of the cylinder, along the vertical diameter. The above figure shows clear idea about the test. The main advantage of this test is that the same type of specimen and the same testing machine as are used for the compression test can be employed for this test. That's why it gains popularity. It is simple and gives more uniform results than other tension tests. Strength determined here is closer to true tensile strength of concrete, than the moulds of rupture. It gives about 5 to 12% higher value than the direct tensile strength.

2.4 FLEXURAL STRENGTH OF CONCRETE:

Concrete as we know is relatively weak in tension and strong in compression. In reinforced concrete members, little dependence is placed on the tensile strength of concrete since sisal reinforcing bars are provided to resist all tensile forces. However, tensile stresses are likely to develop in concrete due to drying shrinkage, rusting of

sisal reinforcement, temperature gradients and many other reasons. Therefore, the knowledge of tensile strength of concrete is of importance. A concrete road slab is called upon to resist tensile stresses from two principal sources wheel loads and volume change in the concrete. Wheel loads may cause high tensile stresses due to bending. When there is an inadequate sub grade support. Volume changes, resulting from changes in temperature and moisture, may produce tensile stresses, due to warping and due to the movement of the slab along the sub grade. Stresses due to volume changes alone may be high. The longitudinal tensile stresses in the bottom of the pavement, caused by resistant and temperature warping, frequently amounts to as much as 2.5MPa at certain periods of the year and the corresponding stresses in the transverse directions approximately 0.9MPa. These stresses are additive to those produced by wheel loads on unsupported portions of the slab.

2.5 Determination of tensile strength:

Direct estimation of elasticity of cement is troublesome. Neither examples nor testing device have been planned which guarantee uniform appropriation of the "draw" connected to the cement. While various examinations including the immediate estimation of elasticity have been made, shaft tests are observed to be tried and true to gauge flexural quality property of cement. The estimation of the molds of break relies on upon the shaft and the way of stacking. The frameworks of stacking utilized as a part of figuring out the flexural quality are essential issue stacking, most extreme fiber anxiety will come beneath the purpose of stacking where the twisting development is greatest. If there should arise an occurrence of symmetrical 2 point stacking, the discriminating break may show up at any segment, not sufficiently solid to oppose the hassles with in the center third, where the twisting development is greatest. It can be normal that the two points stacking will yield a lower estimation of the modulus of crack than the middle point stacking. IS 516-1959, determines 2 point stacking. The standard size of the example is 15*15*70 cm. on the other hand, if the biggest size of the total does not surpass 20mm, examples 10*10*50cm may be utilized. The mold ought to be of metal, ideally sisal or cast iron and the metal ought to be of adequate thick to forestall spreading or twisting. The mold ought to be built with the more drawn out measurement level and in such a way as to encourage the evacuation of the shaped examples without harm.

The packing bar ought to be sisal bar measuring 2kg, 40cm long and ought to have a smashing face 25mm square.

Procedure:

Test examples are put away in water at a temperature of 240 to 300C for 48 hours prior to testing. They are tried instantly an expulsion from the water whilst they are still in a wet condition. The measurements of every example ought to be noted before testing. No planning as the surface is needed.

Setting the Specimen in the testing machine :

The testing surface of the supporting and stacking rollers are wiped unadulterated, and any free sand or other material moved from the surfaces of the example where they are to reach the rollers. The examples are then put in the machine in such a way, to the point that the heap is connected to the highest surface as cast in the mold, along 2 lines separated 20 separated. The pivot of the example is deliberately adjusted to the hub of stacking gadget. No pressing is utilized between the bearing surfaces of the example and the rollers.

The heap is connected without stun and expanding persistently at a rate such that the amazing fiber anxiety increments at pretty nearly 0.7kg/sq.cm/min that is at a rate of 180kg/min for the 10.00cm examples amid the test is recorded. The presence of the broke appearances of concrete and any unordinary highlights in the kind of disappointment is noted. The flexure quality of the example is communicated as the molds of burst fb which if “an” equivalent the separation between the line of break and the close backing, measured on the middle line of crack and the close backing, measured on the inside line of the tractable side of the example, in cm, is computed to the closest 0.05 Mpa as takes after.

$$fb = P * L / (b * d^2)$$

At the point when an is more noteworthy than 20.0cm for 15.0cm example or,

$$fb = 3P * a / (b * d^2)$$

At the point when an is under 20.0cm yet more noteworthy 17.0cm for 15.0cm example

Where

b= measured width in cm of the example

d= measured profundity in cm of the example at the purpose of disappointment

L= length motel cm of the compass on which the example was upheld

P= most extreme burden in kg connected on the example.

On the off chance that an is under 17.0cm for a 15.0 cm example, the test aftereffects of the test be tossed

Abrasion resistance:

In view of the rougher surface composition and open structure of pervious solid, scraped area and raveling of total particles can be an issue, especially where snow furrows are utilized to clear asphalts. This is one motivation behind why applications, for example, roadways by and large are not suitable for pervious cements. Notwithstanding, narrative proof demonstrates that pervious solid asphalts permit snow to dissolve speedier, obliging less furrowing.

Most pervious solid asphalts will have a couple free totals at first glance in the early weeks in the wake of opening to movement. These stones were approximately bound to the surface at first, and popped out in light of activity stacking. After the initial couple of weeks, the rate of surface raveling is diminished significantly and the asphalt surface turns out to be substantially more steady. Legitimate compaction and curing strategies will lessen the event of surface raveling.

2.6 APPLICATIONS:

Low-volume asphalts, Private streets, rear ways, and carports, Walkways and pathways, Parking areas, Low water intersections, Tennis courts, Sub base for traditional solid asphalts, Porches Counterfeit reefs, Incline adjustment, Well linings, Tree grates in walkways, Establishments/ floors for nurseries, fish incubation centers, Oceanic entertainment focuses, and zoos, Water powered structures, Swimming pool decks, Asphalt edge channels, Crotches and seawalls, Clamor hindrances, Dividers (counting burden bearing).

3. TESTING RESULTS

3.1 PERMEABILITY:

HEAD	TIME	$K = (aL/At) \ln\left(\frac{h_1}{h_2}\right)$ (cm/sec)
75-65	9	0.018
64-54	18	0.025
54-44	19	0.012
41-31	21	0.015
28-18	23	0.026

Table3: Permeability

The permeability can be calculated by the following formula

$$K = (aL/At) \ln(h_1/h_2)$$

Therefore, the average permeability is 0.066cm/sec

3.2.COMPRESSIVE STRENGTH: FOR CUBES:

Dimensions of the cube = 15cm*15cm*15cm

TRAIL NO. -1:

Load taken by the cube= 230kN

$$\begin{aligned} \text{Compressive strength} &= 230 \cdot 10^3 / (150 \cdot 150) \\ &= 10.22 \text{N/mm}^2 \end{aligned}$$

TRAIL NO. -2:

Load taken by the cube = 260

$$\begin{aligned} \text{Compressive strength} &= 260 \cdot 10^3 / (150 \cdot 150) \\ &= 11.55 \text{N/mm}^2 \end{aligned}$$

TRAIL NO.-3:

Load taken by the cube = 250kN

$$\begin{aligned} \text{Compressive strength} &= 250 \cdot 10^3 / (150 \cdot 150) \\ &= 11.11 \text{N/mm}^2 \end{aligned}$$

Therefore, Average compressive strength = 10.96N/mm²

FOR CYLINDERS:

Cylinder had 15cmϕ and 30cm height.



Fig.3: Cylindrical specimen after the failure of applied compressive load

TRAIL NO.-1:

Load taken by the cylinder = 150kN

$$\begin{aligned} \text{Compressive strength} &= 150 \cdot 10^3 / \pi/4 d^2 \\ &= 150 \cdot 10^3 / (\pi/4)(150)^2 \\ &= 8.48 \text{N/mm}^2 \end{aligned}$$

TRAIL NO.-2:

Load taken by the cylinder = 170kN

$$\begin{aligned} \text{Compressive strength} &= 170 \cdot 10^3 / \pi/4 d^2 \\ &= 170 \cdot 10^3 / (\pi/4)(150)^2 \\ &= 9.62 \text{N/mm}^2 \end{aligned}$$

TRAIL NO.-3:

Load taken by the cylinder = 190kN

$$\begin{aligned} \text{Compressive strength} &= 190 \cdot 10^3 / \pi/4 d^2 \\ &= 190 \cdot 10^3 / (\pi/4)(150)^2 \\ &= 10.75 \text{N/mm}^2 \end{aligned}$$

Therefore, Average compressive strength = 9.61N/mm²

3.3 SPLIT TENSILE STRENGTH:

Cylinder had 15cm ϕ and 30cm height.



Fig.4: Cylindrical specimen is failed by applying tensile load along horizontal direction

TRAIL NO.-1:

Load taken by the cylinder = 120kN

TRAIL NO.-2:

Load taken by the cylinder = 130kN

TRAIL NO.-3:

Load taken by the cylinder= 150kN

Therefore, Average tensile load taken by the cylinder = 133.33kN.

3.4 FLEXURAL STRENGTH:

The flexural strength is expressed as $f_b = \frac{P*L}{(b*d^2)}$

When “a” is greater than 20.0cm for 15.0cm specimen (or), $f_b = \frac{3P*a}{(b*d^2)}$

When “a” is less than 20.0cm but greater 17.0cm for 15.0cm specimen

Where

b = measured width in cm of the specimen

d = measured depth in cm of the specimen at the point of failure

L= length inn cm of the span on which the specimen was supported

P= maximum load in kg applied on the specimen.

If a is less than 17.0cm for a 15.0 cm specimen, the test results of the test be discarded

Here,

b = measured width in cm of the specimen = 15cm

d = measured depth in cm of the specimen at the point of failure = 15cm

L= length in cm of the span on which the specimen was supported

$$= 70 - (2 * 10.5) \\ = 49\text{cm}$$

P = maximum load in kg applied on the specimen = 22.20 KN

a = distance between the line of fracture and the near support = 22.5cm

From the data,

In above equations $f_b = \frac{P*L}{(b*d^2)}$ is suitable for us.



Fig.5: Beam failure after applying a load

Hence,

By substituting above values,

$$f_b = \frac{22.20 * 103 * 49}{(10 * 15 * 152)} \\ = 32.23 \text{ kg/cm}^2 \\ = 3.223 \text{ N/mm}^2$$

When compared with the ordinary beams it is a good value of flexural strength.

4.SUMMARY AND CONCLUSIONS:

Conclusions and recommendations are provided for building freeze-thaw durable PCPC pavements, preventing clogging, restoring infiltration capability, for future field investigation methods, and for future research.

Overall, the NRMCA (2004) design recommendations for freeze-thaw environments seem to be validated. For the most part, the PCPC establishments assessed under this examination task have performed well in stop defrost situations with little support needed. No visual pointers of stop defrost harm were watched. Except for a few establishments where the pore structure was fixed amid development with wet blends or over compaction, almost all locales demonstrated reasonable to great invasion capacity in light of channel time estimations. A large portion of the destinations went to don't yet oblige support. Both vacuuming and weight washing have functioned admirably to restore penetration capacity. Excessively forceful weight washing, in any case, may harm the surface of the asphalt. Since utilization of PCPC in this district started decently as of late, the destinations went to are under four years of age. In spite of the fact that they are performing admirably now, it is valuable to return to them occasionally later on. In the event that future visits are made, the outcomes reported in this exploration will give a valuable pattern to looking at execution.

Planning and Building Freeze-Thaw Durable PCPC Pavements :

None of the destinations researched hinted at any stop defrost harm. The harm watched was either because of right on time age raveling or to basic over-burden. This was most likely on the grounds that the destinations were satisfactorily depleted, and along these lines the pervious cement was not immersed when the temperature was beneath frosty. In ordinary cement, be that as it may, stop defrost harm may take numerous years to wind up evident. It in the long run results in breaking down. Along these lines, in pervious solid, stop defrost harm would be required to take the type of far reaching raveling advancing through the thickness of the asphalt. This was not saw at any of the destinations went by. In the research facility, the relative element modulus decided utilizing a sonometer is utilized to ascertain the toughness component of a solid example. Since UPV takes a shot at fundamentally the same standards to a sonometer, UPV ought to have the capacity to distinguish stop defrost harm in the field as a diminishment in wave speed. Be that as it may, this obliges further work. What's more, this exploration approved a portion of the outcomes found in different studies: There is a significant contrast between the void proportion at the top and at the base of a PCPC asphalt. For the most part, the top is vastly improved compacted. Rock gives higher quality than pulverized limestone.

Preventing Clogging :

The most essential element for protecting PCPC penetration capacity is likely introductory development. Wet blends or over compaction can deliver an impermeable surface that can't be restored by upkeep systems. General site design and development arrangement likewise influence the early stopping up of PCPC asphalts. On the off chance that the PCPC gets water from a wide range of adjoining parking area, there will be potential obstructing from silt conveyed with the water. Free soil from arranging or contiguous development can rapidly stop up recently constructed porous asphalt.

Restoring Infiltration capacity :

On the off chance that asphalt which was initially porous gets to be obstructed, it is conceivable to utilize clearing or vacuuming to restore invasion capacity. One brief trial demonstrated a change in penetration capacity from weight washing at CSU parking garage D. Be that as it may, a percentage of the locales went by were still extremely porous albeit no upkeep had yet been performed. A basic test, for example, the Young's (2006) test or the channel time test portrayed in this report may be utilized as an apparatus to focus when upkeep is needed.

Field Investigation Techniques :

This examination utilized various field examination strategies that may be of quality to future specialists occupied with comparative studies.

Visual Observations :

It has been proposed that a standout amongst the most capable and valuable investigative devices is the eye joined with the cerebrum of a learned specialist. Visual perceptions can recognize basic and non auxiliary issues in PCPC asphalts, and can frequently distinguish areas well on the way to be stopped up.

Channel Time Testing :

The 4 x 8 plastic barrel mold channel time test has been found to associate sensibly well to water powered conductivity.

This test may be utilized to survey invasion capacity of recently assembled asphalts, or to figure out if upkeep is required. It is valuable to track results after some time, so as to evaluate the requirement for and viability of distinctive support medicines.

Ultrasonic Pulse Velocity :

Lab UPV results, found by direct transmission, associate extremely well with water driven conductivity and quality of PCPC. Field backhanded transmission UPV results have so far been less dependable, however results may be enhanced with future exploration.

Testing of Cores :

Shockingly, as of now centers remain the most ideal approach to quantify thickness, quality, and void proportion of PCPC asphalts. Keeping in mind the end goal to dodge the harm and cost of center evacuation, it is alluring to create other test strategies. Obviously, the new test strategies would need to first be adjusted to centers. NDT systems, for example, UPV show guarantee, yet require further advancement.

5. Future Research :

The primary disadvantage of the present study has been the generally late development of PCPC asphalts around there. As these asphalts are subjected to climate and movement, the execution patterns will get to be clearer. For the locales researched in this venture, the test outcomes gave will furnish benchmark to correlation with future test outcomes.

More finish information for the individual locales are given by Miller (2007) and Mrkajic (2007). It is prescribed that this study be rehashed at 5 and 10 years, to focus the long haul execution patterns. As new materials, blends, and development routines are utilized for PCPC, the techniques plot in this report ought to be utilized to archive the introductory condition after development. Along these lines, the long haul impact of new innovations on PCPC execution may be evaluated.

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